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GRISWOLD'S
RAILROAD ENGINEERS' *B. F. Bush*
POCKET COMPANION
For the Field.

COMPRISING

RULES FOR CALCULATING DEFLEXION DISTANCES AND ANGLES,
TANGENTIAL DISTANCES AND ANGLES, AND ALL
NECESSARY TABLES FOR ENGINEERS;

ALSO,

THE ART OF LEVELING FROM PRELIMINARY SURVEY TO THE
CONSTRUCTION OF RAILROADS, INTENDED EXPRESSLY
FOR THE YOUNG ENGINEER

TOGETHER

WITH NUMEROUS VALUABLE RULES AND EXAMPLES.

BY W. GRISWOLD.

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Northern District of New York.

P R E F A C E.

In offering this book to the patronage of the Assistant Engineer, I would wish to remark, that the book is composed of notes that I have long been collecting.

Every Engineer has his private book of Rules, that should he want for memory in the field, he has only to refer to his book.

This book I have intended for the same object.

For the benefit of the young Engineer, I have inserted the art of leveling, running levels (as it is termed) in plain language, from preliminary surveys to the construction of a railroad; the manner of taking cross sections of the road bed, and setting slope stakes, with its rules. Every feature of the book has a tendency to attract the attention of both the Assistant and the young Engineer.

Tables that would be more used by the Assistant Engineer, are inserted, which can be relied upon as correct, as I have taken them from reliable authors.

In the art of leveling, I have made no allowance for the Earth's curvature, as in practice upon railroads no allowance is ever made.

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RAILROAD ENGINEER'S

POCKET COMPANION

FOR THE FIELD.

EXPLANATION OF LETTERS AND TERMS.

P. C. Point of curve. *E. C.* End of curve.

T. P. Tangent point.

1 Station is equal to 100 feet.

A Plus Station is any number of feet less than 100.

B. S. Back sight. *F. S.* Fore sight.

Int. S. Intermediate sight. *H. Ins.* Height of instrument.

CURVATURE.

To find the radius of curves, from the deflexion angles, from chord to chord. (Chord 100 ft.)

RULE 1.

As angle of deflexion

Is to the length of the chord,

So is 57.3 to radius.

To find radius of curves, from the deflexion distance, from chord to chord. (Chord 100 ft.)

RULE 2.

The square of the chord, divided by the deflexion distance.

EXAMPLE.—Deflexion distance = 3.1416 ft.;
 Square of chord 10,000;
 3.49 10,000 (2865, radius.

To find the radius of a curve, from the deflexion angle, on chord of 100 ft.

RULE 3.

Divide the radius of a one degree curve (5,730) by the degrees of deflexion of 100 ft.

To find radius of a segment of a circle.

RULE 4.

Square of half the chord, added to the square of versed sine, = square of chord of half the arc; and square of chord of half the arc, divided by versed sine, = diameter; $\frac{1}{2}$ = radius.

When the angle at vertex is given, and radius, to find the tangent point.

RULE 5.

Multiply nat. tangent of half the whole angle in the curve, by radius of curve; will equal distance from vertex to tangent point.

When the distance from vertex to tangent point, and angle given, to find radius.

RULE 6.

Subtract the angle $a b c$, (Fig. 1) which is half the angle $a b d$, from 90° ; the remainder will be the angle $b c a$.

Then say: As nat. sine of $b c a$ is to nat. sine of $a b c$, so is $a b$ or $b d$ to the radius.

Having given the angle $a b d$, (Fig. 1) it is required to find the point a or d , at which to commence a curve, of a given radius.

RULE 7.

Subtract half the angle $a b d$ from 90° , the remainder will be the angle $b c a$ or $b c d$; then take the natural tangent of $b c a$ or $b c d$, and multiply it by the given radius; the product will be $b a$ or $b d$.

Having the given radius (Fig. 1) $a c$, or deflexion angle for 100 ft., of a curve, and the angle $a b d$, it is required to find the number of chords of 100 ft. that will constitute the curve.

RULE 8.

Subtract the angle $a b d$ from 180° , and divide the remainder by the angle of deflexion in 100 ft.

Having the angle at vertex (Fig. 1) $e b d$, (which is the number of degrees in the curve,) and deflexion angle for 100 ft., to find the number of chords in that curve.

RULE 9.

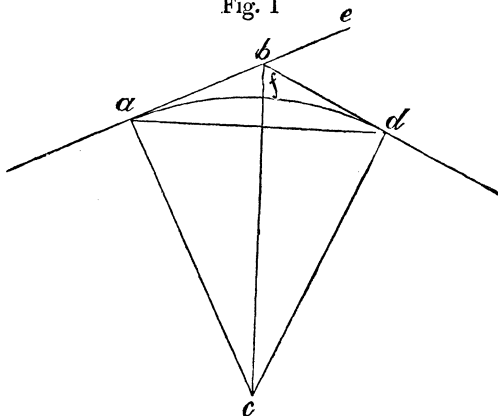
Divide the number of degrees at vertex by deflexion angle.

With the distance $a b$ or $b d$, and radius $a c$ given, to find the distance from f to b , (Fig. 1.)

RULE 10.

The square of the distance from vertex to $P. C.$ divided by twice the radius.

Fig. 1



EXAMPLE.—Suppose the distance from a to $b = 511$ ft., and radius $= 1,910$ ft.,

Then $511^2 = 261,121 \div 2 \times 1,910 = 68.2$, Answer.

NOTE.—The square of any distance, divided by twice radius, will equal the distance from tangent to curve, very nearly.

When the distance ab or bd is given, and distance fb , (Fig. 1) to find radius.

RULE 11.

Divide the square of the distance ab or bd by the distance fb , equals twice the length of radius, $\frac{1}{2} =$ radius.

EXAMPLE.—Suppose the distance fb equals 68.2, and ab or bd equal 511.

STATEMENT.— $511^2 = 261,121 \div 68.2 = 3,820 \div 2 = 1,910$, radius.

To find the radius corresponding to any given angle of deflexion, and to equal chords of any given length.

RULE 12.

Subtract the angle of deflexion from 180° ; then say: as nat. sine of angle of deflexion, is to nat. sine of half the remainder, so is the given chord to the radius required.

EXAMPLE.—Let the angle of deflexion be 2° , and the chord 100 ft., required the radius.

Then $2^\circ - 180^\circ = 178^\circ \div 2 = 89^\circ$.

N. S. 2° . N. Sine 89° . Chord.

STATEMENT.— $0.0349 : .999848 :: 100 : 2865$, radius.

To find the circumference of a circle, when the diameter is given, or the diameter, when the circumference is given.

RULE 13.

Multiply the diameter by 3.1416, equals circumference; or, divide the circumference by 3.1416, equals diameter.

2d. As 7 is to 22,

So is the diameter to the circumference.

Or, as 22 is to 7,

So is the circumference to the diameter.

To find the length of an arc or circle, containing any number of degrees.

RULE 14.

Multiply the number of degrees in the given arc,

by 0.0087266, and the product by the diameter of the circle.

NOTE.—The circumference of a circle, whose diameter is 1, is 3.1416; it follows, that if 3.1416 be divided by 360°, the quotient will be the length of an arc of 1 degree, = 0.0087266.

REMARK.—When the arc contains degrees and minutes, reduce the minutes to a decimal of a degree.

To find the length of any arc of a circle.

RULE 15.

Subtract the chord of the whole arc from 8 times the chord of half the arc, and $\frac{2}{3}$ of the remainder is the length of the arc, nearly.

When the chord of the arc, and the chord of half the arc, are given.

RULE 16.

From the square of the chord of half the arc, subtract the square of half the chord of the entire arc; will equal the square of the versed sine; extract the square root; will equal versed sine—the versed sine and the chord given—the square of $\frac{1}{2}$ the length of the chord, added to the square of the versed sine, and square root of the remainder, will equal chord of $\frac{1}{2}$ the arc; multiply the remainder by 8, subtract the chord of the whole arc, and divide by 3, equals length of arc.

To find the circumference of an ellipses.

RULE 17.

Half the sum of the two diameters, multiplied by 3.1416; the product will equal circumference.

TABLE OF RADII—CHORDS 100 FT.

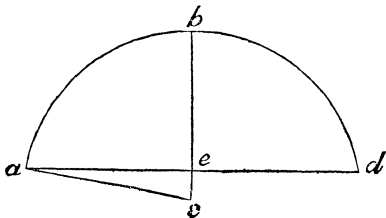
Angle of Deflexion.	Radius in Feet.	Angle of Deflexion.	Radius in Feet.	Angle of Deflexion.	Radius in Feet.	Angle of Deflexion.	Radius in Feet.
0	15	8	15	16	15	24	15
30	22920	30	695.1	30	353.8	30	238.0
45	11460	45	674.6	45	348.4	45	235.6
1	7640	9	655.5	17	343.3	25	233.3
15	5730	15	637.3	15	338.3	15	231.0
30	4584	30	620.2	30	333.7	30	228.7
45	3820	45	603.8	45	328.7	45	226.5
2	3274	10	588.4	18	324.8	26	224.3
15	2865	15	573.7	15	319.6	15	222.3
30	2547	30	559.7	30	315.2	30	220.6
45	2292	45	546.4	45	311.0	45	218.0
3	2084.0	11	533.8	19	306.9	27	216.0
15	1910	15	521.7	15	302.9	15	214.2
30	1763	30	510.1	30	299.4	30	212.2
45	1637	45	499.1	45	295.3	45	210.3
4	1528	12	488.5	20	291.5	28	208.5
15	1433	15	478.3	15	287.9	29	206.7
30	1348	30	468.7	30	284.4	30	199.7
45	1274	45	459.3	45	280.9	31	193.2
5	1207	13	450.3	21	277.6	32	187.1
15	1146	15	441.7	15	274.4	33	181.4
30	1092	30	433.4	30	271.1	34	176.0
45	1042	45	425.5	45	268.0	35	171.0
6	996.8	14	417.7	22	265.0	36	166.3
15	955.4	15	410.3	15	262.0	37	161.8
30	917.0	30	403.1	30	260.0	38	157.6
45	882.0	45	396.2	45	257.4	39	153.6
7	849.3	15	389.6	23	254.6	40	149.8
15	819.0	15	383.1	15	250.8	45	146.2
30	790.8	30	376.9	30	248.1		136.5
45	764.5	45	370.8	45	245.5		
8	739.9	16	365.0	24	242.9		
	716.8		359.3		240.5		

To find the radius corresponding to any given angle of deflexion, and to equal chords of any given length.

RULE 18.

Subtract the angle of deflexion from 180° ; then say: as nat. sine of angle of deflexion is to nat. sine of half the remainder, so is the given chord to the radius required.

Fig. 2.



With the chord and versed sine given, to find the radius.

RULE 19.

The square of half the chord divided by versed sine; to which add the versed sine, and divide by 2.

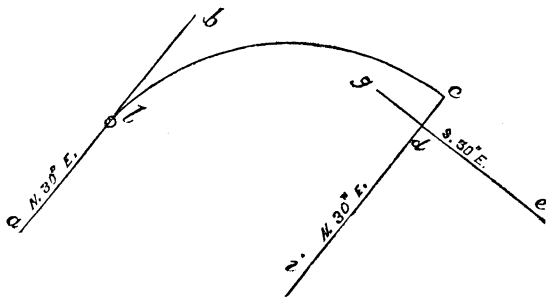
EXAMPLE.—Suppose we have an arc (Fig. 2) with a chord $a d$ of five feet, and versed sine $e b$ two feet, what is the radius $a c$?

STATEMENT.— $5 \div 2 = 2.5^2 = 6.25 \div 2 = 3.125 + 2 = 5.125 \div 2 = 2.5625$, radius $a c$.

We have two tangents with their courses given. We wish to unite those tangents, with a curve of a given radius.

Suppose we have a tangent whose course is $N. 30^\circ E.$, (Fig. 3) which we wish to unite with a 3° curve to a tangent whose course is $S. 50^\circ E.$ We here find we have the difference of courses to be 100° . According to Rule 8, page 7, and Rule 20, page 14, we have $3,333\frac{33}{100}$ ft. to run. We start on the first given tangent, and run $3,333\frac{33}{100}$ ft. If our curve does not form a tangent of the line $g e$, but touches the point c , we measure in a line the same course of the first tangent, $N. 30^\circ E.$, to its intersection, which distance you measure backward or forward for $P. C.$

Fig. 3.



EXAMPLE.—We have the tangent $a b$, $N. 30^\circ E.$, and tangent $e g$, $S. 50^\circ E.$; we wish to join those two tangents with a 3° curve.

STATEMENT.— $T. N. 30^\circ E.$ and $T. S. 50^\circ E. = 100^\circ$, angle of deflexion, which makes 100° in the curve; consequently, the number of feet in the curve

(chords 100 ft.) = $100^\circ \div 3 = 33$ stations and $33\frac{33}{100}$ ft. = $3,333\frac{33}{100}$ ft. We start from the tangent *a b*, at the point *l*, and run $3,333\frac{33}{100}$ ft., turning off for a 3° curve, and find, when arriving at our tangent, we are 250 ft. from the line, as *d c*; we then return and measure the same distance on the tangent *a b* from *l* to *P. C.*

With the angle at vertex given, and degree of curvature, to find how many feet constitutes the curve.

RULE 20.

Divide the number of degrees at vertex, by degree of curvature.

EXAMPLE.—We have the angle at vertex = 100° , and degree of curvature = 3° .

STATEMENT.— $100^\circ \div 3^\circ = 33$ stations and $33\frac{33}{100}$ ft. = $3,333\frac{33}{100}$ ft.

If there is any number of feet less than 100 ft., in your curve, to find how many degrees and minutes to turn off.

RULE 21.

Say: as 100 ft. is to the number of feet you wish to run, so is the number of degrees and minutes to the number of degrees and minutes you wish to find.

EXAMPLE.—Suppose you turn off in every 100 ft., $1^\circ 30'$, how much will it be necessary to turn off in 33 ft.?

STATEMENT.— $100:33::1^\circ 30':30'$, Answer.

Suppose you have a less number of degrees and minutes, than you turn off in 100 ft., to find the number of feet necessary to measure.

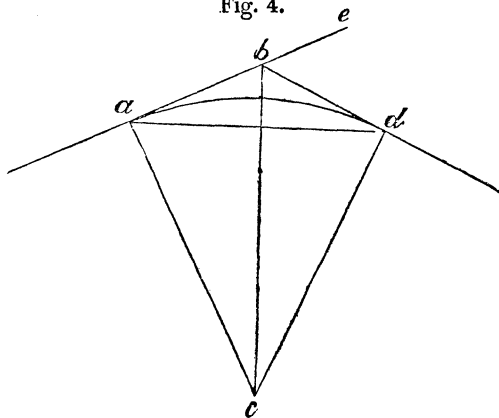
RULE 22.

As the whole number of degrees and minutes is to the number of degrees and minutes you wish to turn off, so is the chord, 100 ft., to the number of feet required.

EXAMPLE.—We turn off in 100 ft. $1^{\circ} 30'$, we wish to find the number of feet to measure for $30'$.

STATEMENT.— $1^{\circ} 30' : 30' :: 100 : 33$, Answer.

Fig. 4.



With the angle $a b d$, (Fig. 4) and distance $a b$ given, to find radius $a c$.

RULE 23.

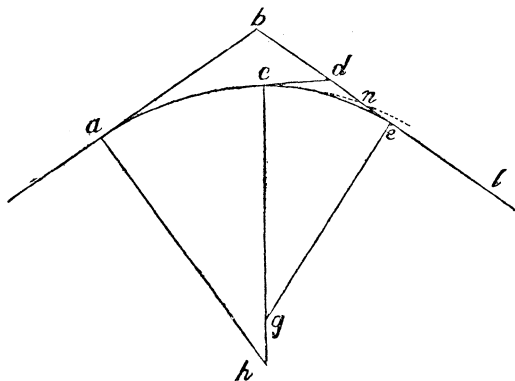
Half the angle $a b d$ taken from $90^{\circ} =$ angle $a c b$.

Then say: as nat. sine of $a c b$ is to nat. sine of $a b c$, so is the given side $a b$ or $b d$ to the radius $a c$.

NOTE.—This rule is often used in compounding curves, where the curve you have run does not fit the tangent, by measuring from a given point, on a tangent, to curve already run, to the tangent you wish to connect, as $b\ l$ (Fig. 5) and measuring the angle $c\ d\ l$, and proceed according to rule 23.

Thus in Fig. 5, we run our curve to n , and find that it does not come in tangentially to the tangent $b\ l$, therefore to save loss of time, in long curves, we retrace our steps to the point c , and measure tangentially to curve $a\ c$, as $c\ d$ to the tangent $b\ l$, and measure the angle $c\ d\ l$, and form a new radius, as $c\ g$ or $e\ g$.

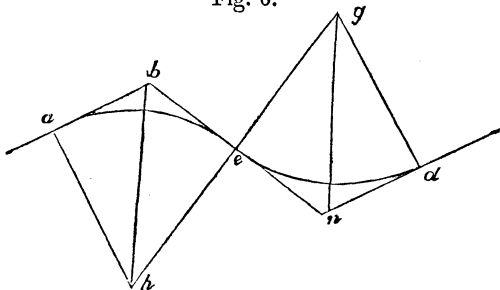
Fig. 5.



We oftentimes have two different angles in a line, and in such close proximity that it is required to put in reversed curves (Fig. 6) that will connect with the greatest possible radius; we then wish to find

the greatest radius $a h$ and $e g$ that will connect the tangents with a reversed curve.

Fig. 6.



RULE 24.

Half the angle $a b e$ taken from 90° leaves the angle $b h e$ or $a h b$, and half the angle $b n d$ taken from 90° leaves the angle $e g n$. From the table of nat. tangent take the nat. tangent of $b h e$ or $a h b$ and nat. tangent of the angle $e g n$ and add them together.

Then say: as the sum of these two nat. tangents is to the nat. tangent of $b h e$, so is the distance $b n$ to $b e$.

Again, in the triangle $b h e$, as the nat. sine of the angle $b h e$, opposite the given side $b e$ just found, is to the nat. sine of the angle $h b e$, opposite the required side $h e$, so is $b e$ to $h e$, the radius required.

EXAMPLE.—Let the angle $a b n$ be $71^\circ 40'$, the angle $b n d$ $129^\circ 15'$, and the distance $b n$ be 950 ft., what is the length of the radius $h e$ or $e g$?

STATEMENT 1st.— $71^{\circ} 40' \div 2 = 35^{\circ} 50' - 90 = 54^{\circ} 10'$.

$$129^{\circ} 15' \div 2 = 64^{\circ} 37\frac{1}{2}' - 90 = 25^{\circ} 22\frac{1}{2}'.$$

$$\text{Nat. tangent of } 54^{\circ} 10' = 1.3848.$$

$$\text{Nat. tangent of } 25^{\circ} 22\frac{1}{2}' = 0.4743 + 1.3848 = 1.8591.$$

Sum. N. tang. $54^{\circ} 10'$ $b n$ $b e$

$$\text{Then as } 1.8591 : 1.3848 :: 950 \text{ ft.} : 707.63 \text{ ft.}$$

$$\text{Again, } 950 - 707.63 = 242.37 \text{ ft.} = e n.$$

Sine $b h e$. N. sine $h b e$.

STATEMENT 2d.— $0.8107 : .5854 :: 707.63 : 510.97$, radius required.

Hence, we have the distance $h e$ and $e g = 510.97$ ft., and distance $b e$ 707.63 ft., and distance $e n$ 342.37 ft., and degree of curvature equal to $11^{\circ} 16'$ for chords of 100 f'

The radius of a curve is always at right angles with its tangent.

When running curves with a compass, or transit instrument, always turn off on the vernia, one-half the number of degrees as contains degrees of curvature; because when running with an instrument, you are running tangential angles instead of deflexion angles, and the tangential angle equals one-half the deflexion angle.

ORDINATES.

To find ordinates on chords of 100 ft.

RULE 1.

The product of the segment, divided by twice the radius.

EXAMPLE.—Suppose the radius = 2·865 ft.; what would be the ordinate for 25 ft.? (Chords 100 ft.)

$$25 \times 75 \div 5,730 = 0\cdot327.$$

Rule for getting the ordinate for 50 ft. and 25 ft. approximately.

RULE 2.

For an ordinate of 50 ft., divide the deflexion distance for 100 ft. by 8. For 25 ft. three-fourths of the ordinate for 50 ft.

EXAMPLE.—Suppose the deflexion = 3° , which deflexion distance = $5\cdot235 \div 8 = 0\cdot654$, ordinate for 50 ft., and three-fourths of $0\cdot654 = 0\cdot491$, ordinate for 25 ft.

To find the middle ordinate to any given radius, and to any given chord.

RULE 3.

From the square of the radius, subtract the square of half the chord, and take the square root of the remainder from the radius = middle ordinate.

EXAMPLE.—What is the length of the middle ordinate $d e$, (Fig. 1) the radius $a c$ being 2·5625, and chord $a b$ 5 ft.

STATEMENT.— $2\cdot5625^2 - 2\cdot5^2 = \sqrt{316406} = \cdot5625$
— $2\cdot5625 = 2$ ft., middle ordinate.

TABLE OF ORDINATES — CHORDS 100 FT.

Angle of Deflexion.	Length of Ordinates in Feet.									
	50	45	40	35	30	25	20	15	10	5
0										
5	.018	.018	.017	.016	.015	.014	.012	.009	.006	.003
10	.036	.036	.035	.033	.031	.027	.023	.019	.013	.007
15	.054	.054	.052	.049	.046	.041	.035	.028	.019	.010
20	.073	.072	.070	.066	.061	.055	.047	.037	.026	.014
25	.091	.090	.087	.082	.076	.068	.058	.046	.032	.017
30	.109	.108	.105	.099	.092	.082	.070	.055	.039	.020
35	.127	.126	.123	.116	.108	.096	.082	.065	.045	.024
40	.145	.144	.140	.133	.123	.110	.093	.074	.052	.027
45	.163	.161	.157	.149	.137	.123	.105	.083	.058	.031
50	.182	.180	.175	.166	.153	.138	.117	.092	.065	.034
55	.200	.198	.192	.182	.168	.151	.128	.102	.071	.038
1										
5	.218	.216	.209	.198	.183	.164	.140	.111	.078	.041
10	.236	.234	.226	.215	.198	.178	.152	.120	.085	.044
15	.254	.252	.244	.231	.214	.191	.163	.130	.091	.048
20	.273	.270	.261	.248	.229	.205	.175	.139	.098	.051
25	.291	.288	.279	.264	.244	.218	.187	.148	.104	.055
30	.309	.306	.296	.281	.259	.232	.198	.157	.111	.058
35	.327	.324	.314	.297	.275	.246	.210	.167	.117	.062
40	.345	.342	.331	.314	.290	.259	.221	.176	.124	.065
45	.364	.360	.349	.330	.305	.273	.233	.185	.130	.069
50	.382	.378	.366	.347	.321	.287	.245	.195	.137	.072
55	.400	.396	.384	.364	.336	.300	.256	.204	.144	.076
2										
5	.418	.414	.401	.380	.351	.314	.268	.213	.150	.079
10	.436	.432	.419	.397	.366	.327	.280	.222	.157	.083
15	.454	.450	.436	.413	.382	.341	.291	.232	.163	.086
20	.473	.468	.454	.430	.397	.355	.303	.241	.170	.089
25	.491	.486	.471	.446	.412	.368	.315	.250	.176	.093
30	.509	.504	.489	.463	.428	.382	.326	.260	.183	.096
35	.527	.522	.506	.480	.443	.396	.338	.269	.190	.100
40	.545	.540	.524	.496	.458	.409	.350	.278	.196	.103
45	.564	.558	.541	.513	.474	.423	.361	.288	.203	.107
50	.582	.576	.559	.529	.489	.436	.373	.297	.209	.110
55	.600	.594	.576	.546	.504	.450	.384	.306	.216	.114
3										
5	.618	.612	.594	.562	.519	.464	.396	.315	.222	.117
10	.636	.630	.611	.579	.535	.477	.408	.325	.229	.121
15	.654	.648	.629	.595	.550	.491	.419	.334	.235	.124
20	.673	.666	.646	.612	.565	.504	.431	.343	.242	.128
25	.691	.684	.664	.629	.581	.518	.443	.353	.249	.131
30	.709	.702	.681	.645	.596	.532	.454	.362	.255	.134
35	.727	.720	.699	.662	.611	.545	.466	.371	.262	.138
40	.745	.738	.716	.678	.627	.559	.478	.380	.268	.141
45	.764	.756	.734	.695	.642	.573	.489	.390	.275	.145
50	.782	.774	.751	.711	.657	.586	.501	.399	.281	.148
55	.800	.792	.769	.728	.673	.600	.512	.408	.288	.152
4										
5	.818	.810	.786	.744	.688	.613	.524	.418	.294	.155
10	.836	.828	.804	.761	.703	.627	.536	.427	.301	.159
15	.854	.846	.821	.778	.718	.641	.547	.436	.308	.162
20	.873	.864	.839	.794	.734	.654	.559	.445	.314	.166

TABLE OF ORDINATES — CHORDS 100 FT.

Angle of Deflexion.	Length of Ordinates in Feet.									
	50	45	40	35	30	25	20	15	10	5
4 15	.927	.918	.891	.844	.780	.695	.594	.473	.334	.176
30	.981	.972	.944	.893	.825	.736	.629	.501	.354	.186
45	1.036	1.026	.996	.943	.871	.777	.664	.529	.373	.196
5 15	1.091	1.080	1.048	.993	.917	.818	.699	.557	.393	.207
30	1.146	1.134	1.100	1.042	.963	.859	.734	.585	.413	.217
45	1.200	1.188	1.153	1.092	1.009	.900	.769	.613	.432	.228
6 15	1.255	1.242	1.205	1.141	1.055	.941	.804	.640	.462	.238
30	1.309	1.296	1.258	1.191	1.100	.982	.839	.668	.472	.249
45	1.419	1.404	1.362	1.290	1.192	1.064	.909	.724	.511	.269
7 15	1.473	1.458	1.415	1.339	1.238	1.105	.944	.752	.531	.280
30	1.528	1.512	1.467	1.389	1.284	1.146	.979	.779	.551	.290
45	1.637	1.620	1.572	1.488	1.375	1.228	1.048	.835	.590	.311
8 15	1.746	1.728	1.677	1.587	1.467	1.310	1.118	.891	.629	.332
30	1.855	1.836	1.782	1.687	1.559	1.392	1.188	.946	.669	.353
45	1.965	1.944	1.886	1.787	1.651	1.474	1.258	1.002	.708	.373
9 15	2.074	2.052	1.991	1.887	1.742	1.556	1.328	1.057	.748	.394
30	2.183	2.161	2.096	1.987	1.834	1.637	1.398	1.114	.787	.415
45	2.292	2.269	2.201	2.087	1.926	1.719	1.468	1.170	.827	.436
10 15	2.401	2.377	2.306	2.186	2.018	1.802	1.538	1.226	.866	.457
30	2.511	2.486	2.411	2.236	2.110	1.884	1.609	1.282	.906	.478
45	2.620	2.594	2.516	2.336	2.203	1.967	1.680	1.339	.946	.499
11 15	2.839	2.811	2.726	2.585	2.387	2.132	1.820	1.451	1.025	.541
30	3.058	3.028	2.937	2.785	2.571	2.297	1.961	1.564	1.105	.583
45	3.277	3.245	3.147	2.984	2.756	2.462	2.102	1.676	1.184	.625
12 15	3.496	3.462	3.358	3.184	2.941	2.627	2.243	1.789	1.264	.667
30	3.716	3.680	3.569	3.384	3.125	2.792	2.384	1.902	1.344	.709
45	3.935	3.897	3.779	3.584	3.310	2.958	2.525	2.014	1.424	.751
13 15	4.155	4.115	3.990	3.784	3.495	3.123	2.666	2.127	1.504	.793
30	4.375	4.332	4.201	3.984	3.690	3.288	2.808	2.240	1.583	.836
45	4.595	4.549	4.412	4.184	3.864	3.454	2.950	2.353	1.663	.879
14 15	4.815	4.768	4.624	4.386	4.050	3.620	3.093	2.467	1.744	.922
30	5.035	4.986	4.836	4.587	4.237	3.786	3.236	2.581	1.824	.965
45	5.255	5.204	5.048	4.789	4.423	3.952	3.379	2.695	1.905	1.008
15 15	5.476	5.422	5.260	4.989	4.609	4.119	3.522	2.809	1.986	1.051
30	5.697	5.642	5.473	5.192	4.798	4.286	3.665	2.924	2.068	1.094
45	5.918	5.860	5.685	5.393	4.984	4.454	3.808	3.039	2.150	1.137
16 15	6.139	6.079	5.898	5.595	5.171	4.622	3.952	3.154	2.232	1.181
30	6.361	6.298	6.110	5.796	5.357	4.790	4.095	3.269	2.314	1.224
45	6.582	6.517	6.323	5.999	5.544	4.958	4.239	3.385	2.396	1.268
17 15	6.804	6.737	6.537	6.202	5.733	5.127	4.384	3.502	2.481	1.312
30	7.027	6.957	6.751	6.406	5.922	5.297	4.530	3.619	2.565	1.356
45	7.249	7.178	6.965	6.609	6.111	5.467	4.676	3.737	2.649	1.401
18 15	7.472	7.398	7.179	6.813	6.300	5.637	4.822	3.854	2.733	1.445
30	7.694	7.619	7.393	7.017	6.489	5.807	4.968	3.972	2.817	1.490
45	7.918	7.841	7.609	7.222	6.679	5.978	5.115	4.090	2.901	1.535
19 15	8.143	8.063	7.825	7.427	6.870	6.149	5.262	4.209	2.985	1.581
30	8.367	8.286	8.041	7.633	7.060	6.320	5.410	4.327	3.069	1.626

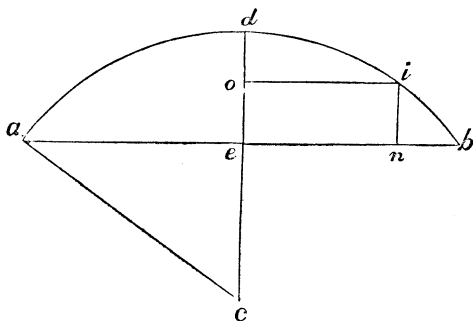
RULE 4.

Subtract the tabular cosine of the tangential angles from 1, and multiply the remainder by the radius. (Chords 100 ft.)

EXAMPLE.—Radius 819 ft., angle of deflexion would be 7° to chord of 100 ft; what will be the length of the middle ordinate?

STATEMENT.—Here tabular cosine of the tangential angle $3\frac{1}{2}^\circ = .998135$, which, subtracted from 1 = $.001865$, which, multiplied by radius, 819 ft., = ordinate, 1.528.

Fig. 1.



Having the middle ordinate $d e$, (Fig. 1) it is required to find any other ordinate, as $i n$.

RULE 5.

Subtract the middle ordinate $d e$, from the radius $a c$, the remainder will be $e c$; from the square of the radius $a c$, subtract the square of the distance $o i$

or $e n$, and extract the square root of the remainder; this square root will be $o c$; subtract $e c$ from $o c$; the remainder will be $o e$, which is equal to $i n$, the required ordinate.

EXAMPLE.—The middle ordinate $d e$ (Fig. 1) of a 100 ft. chord $a b$, to a radius of 819 ft. = 1.52; it is required to find the length of the ordinate $i n$ 20 ft. from the middle one $d e$.

STATEMENT.— $819 - 1.528 = 817.472$.

Again, $819^2 = 670761 - 20^2 = \sqrt{670361} = 818.756 = o c - 817.472 = 1.284$, will equal $o e$ or $i n$, the required ordinate.

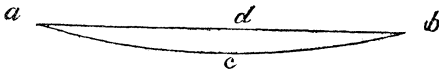
To find middle ordinate approximately. Chord 100 ft.

RULE 6.

Multiply the ordinate of a 1° curve by the deflexion angle of 100 ft. This rule is sufficiently close for curves of not less than 500 ft. radius.

2d. Multiply the chords together, and divide by twice the radius.

Fig. 2.



To find the ordinate for a railroad bar $a c b$ (Fig. 2) 24 ft. long.

RULE 7.

Multiply one-half the length of the rail by one-fourth its length, and divide by the radius.

EXAMPLE.—Rail 24 ft. long, radius 5730.

STATEMENT.— $24 \div \frac{1}{2} = 12 = \frac{1}{2}$ the length of rail.

$24 \div \frac{1}{4} = 6 = \frac{1}{4}$ the length of rail.

Then $6 \times 12 = 72 \div 5730 = 0.01$, ordinate required.

2d. Take one-fourth of the square of the length of the rail, and divide it by twice the radius.

An approximate rule for calculating the middle ordinate of a sub-chord, when the middle ordinate is given. (Chord 100 ft.)

RULE 8.

As the square of the length of the whole chord is to the square of the length of the sub-chord, so is the middle ordinate of the chord to the middle ordinate of the sub-chord.

EXAMPLE.—Chord 100 ft., middle ordinate .218, what will be the middle ordinate of the sub-chord 50 ft.?

STATEMENT.— $100^2 : 50^2 :: .218 : .0545$.

Fig. 3.



In running a curve for track, after the grading is done, it is necessary to put in intermediate ordinates, if the curve exceeds 1° ; (Fig. 3) these intermediates are from 10 to 20 ft. apart, and instead of running these intermediates with an instrument, the best

method is, after your points are put in with an instrument 100 ft. apart, to draw a small cord or twine, as *a b*, and measure off your ordinates with a graduated rod, or with the leveling rod.

NOTE.—Refer to Rule 1, page 19 for intermediates or to table.

When the chord and radius are given, to find middle ordinate. (Chord 100 ft.)

RULE 9.

Divide the square of the chord by eight times the radius.

DEFLEXION DISTANCE.

To find the deflexion distance for 100 ft., with any given radius.

RULE 1.

The square of the chord divided by the radius.

RULE 2.

Divide the constant number 10,000 (chords 100 ft.) by the radius in feet, equals deflexion distance.

To find the deflexion distance for any given radius for chords of 100 ft.

RULE 3.

Divide the given chord by radius, will give the nat. sine of the deflexion angle, which, multiplied by the chord, will equal the required distance.

NOTE.—The tangential distance for 100 ft. is equal to one-half the deflexion distance, and the tangential angle is always equal to one-half the deflexion angle.

measure your distance $f d$, and lay off $a d$ equal to one-half $b c$, or one-half the deflexion distance, as $a d$ is the tangential distance, and the tangential distance is equal to one-half the deflexion distance.

If you wish to put in intermediates, as it frequently occurs, at the end of a curve.

RULE 4.

Find your deflexion distance for 100 ft., string a line, and put in the required ordinate.

To find the deflexion distance for any number of feet less than 100.

RULE 5.

Take the deflexion distance for 100 ft. and multiply it by the required chord, and divide the product by the length of the whole chord, 100 ft., and subtract the ordinate corresponding in feet and degree.

EXAMPLE.—We wish to get the deflexion distance for 25 ft., for a 15° curve.

STATEMENT.—Deflexion distance equals 26.11 ft., therefore:

$$26.11 \times 25 = 652.75 \div 100 = 6.5275.$$

Now the ordinate of a 15° curve for 25 ft. = 2.462, and $6.5275 - 2.462 = 4.0655$, deflexion distance for 25 ft.

NOTE.—The above Rule is sufficiently close for all practical work.

Where it is required to find the deflexion or tangential distance for more than 50 ft., subtract the distance to be found from 100, and find the ordinate corresponding to the remainder in feet.

To find the deflexion point for any number of feet, at commencement of curves and ending, where the distance is less than 100 ft.

RULE 6.

In commencing a curve, multiply the tangential distance in feet by the number of feet in the chord you wish to find, and divide the product by the length of the whole chord, 100 ft., and measure the distance on the end of a 100 ft. chord; then a line drawn from this point to the *P. C.*, the length of the chord measured you desire to find, on this line, is the point of deflexion.

RULE 7.

To end your curve: Take half the deflexion distance for 100 ft., then multiply the remaining distance (which is the tangential distance,) by the number of feet you wish to find, and divide the product by the length of the whole chord, 100 ft., and measure on the tangential distance, the distance just found; then string a line from this point to the last station given, and measure, on this last given line, the distance required, will give the *T. P.* or *E. C.*

To form a tangent to the curve: Measure as many feet more on the tangential distance, and a line drawn from the last given point to *T. P.* or *E. C.* will be the course of the tangent.

EXAMPLE TO RULE 6.—Suppose in commencing a curve we wish to find the deflexion distance of 25 ft. as at *r*, (Fig. 2) for a 15° curve. We take the tangential distance *c f* and multiply it by 25 ft., and divide by 100 ft., (the length of the whole chord,) will equal the distance *c s*; now if we measure in the

line $b s$ 25 ft. from b to r , at r will be the required point. We then measure 100 ft. from r to d , in line with $b r$, and measure the deflexion distance $d e$, equal to twice $c f$, for our next full station. We then measure 100 ft. on the line $r e$ from e to the point h , and measure the distance $h i$ for our next station, so on to the last station.

EXAMPLE TO RULE 7.—Suppose in ending our curve we wish to find the deflexion distance for 25 ft., to conclude the curve; (Fig. 2) suppose i to be the last station in the curve, and the point t 25 ft., to be the $E. C.$; we produce the line $e i$ to k 100 ft. from i , and measure one-half the deflexion distance, $k o = l$, then multiply the distance $k l$ by 25 ft., and divide by the length of the whole chord $i k$, 100 ft., will equal the distance $l m$, and on the line drawn from m to i , 25 ft. measured from i to t , on this line $i m$, will be the required point. To form a tangent to the point t , measure $m y$ equal to $l m$, will form the tangent $t n$ to the curve.

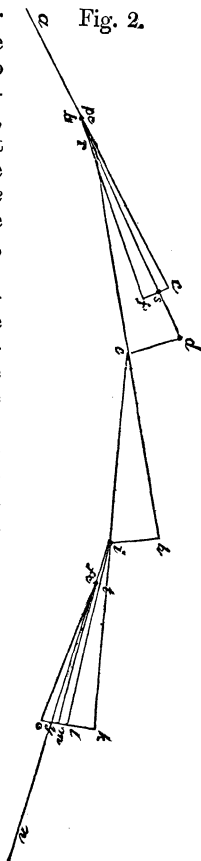


Fig. 2.

TABLE OF DEFLEXION DISTANCES.

Deflexion Angle.	Length of Chords in Feet.			
	100	75	50	25
0° 30'	·872	0·572	0·247	0·136
45	1·308	0·899	0·491	0·204
1° 30'	1·745	1·144	0·654	0·272
45	2·618	1·717	0·982	0·408
2° 30'	3·054	2·003	1·145	0·476
45	3·490	2·290	1·309	0·545
3° 30'	4·363	2·863	1·636	0·681
45	4·799	3·419	1·799	0·749
4° 30'	5·235	3·435	1·963	0·818
45	6·108	4·008	2·290	0·954
5° 30'	6·544	4·295	2·454	1·023
45	6·980	4·581	2·617	1·091
6° 30'	7·853	5·153	2·945	1·227
45	8·289	5·440	3·108	1·295
7° 30'	8·722	5·723	3·270	1·362
45	10·470	6·870	3·926	1·635
8° 30'	12·210	8·011	4·577	1·906
45	13·950	9·152	5·229	2·177
9° 30'	15·680	10·286	5·875	2·446
45	17·430	11·435	6·532	2·720
10° 30'	19·170	12·575	7·184	2·990
45	20·940	13·738	7·850	3·268
11° 30'	22·640	14·848	8·481	3·528
45	24·370	15·980	9·127	3·795
12° 30'	26·110	17·120	9·778	4·065

If two lines vary any number of degrees, to find the distance approximately at their extremities.

RULE 8.

Say; If they vary 1·745 in 1° for 100 ft., it will vary thirty times as much in an angle of 30° for

100 ft.; if it is more than 100 ft., make a second statement.

EXAMPLE.—Suppose we have an angle of 30° and 400 ft. long, what is the distance apart at their extremities?

STATEMENT.—As $1^\circ:30^\circ::1.745:52.35$; 52.35 is the difference for 100 ft.

Then as 100 ft.:400 ft.:52.35:209.4, the difference for 400 ft.

Suppose we run a line, on a given course, with the intention of striking a certain point, and find that we deviate from that point, to find the course of the second line that will unite these two points on a straight line.

RULE 9.

Multiply the difference of variation in feet by 57.3,* and divide the product by the length of the line, the quotient either added or subtracted, as necessity requires, will be the course of the line that will unite the two points together.

EXAMPLE.—Suppose the difference of variation = 209.4 ft., and length of line 400 ft., and course *N.* $29^\circ 59\frac{3}{4}'$ *E.*, what would be the course of the second line, if the point desired is *N. W.* of the line run?

STATEMENT.— $209.4 \times 57.3 \div 400 = 29.9965 = 29^\circ 59\frac{3}{4}'$.

Then course *N.* $29^\circ 59\frac{3}{4}'$ *E.* — $29^\circ 59\frac{3}{4}'$ = course *N.* 0° *E.*

*57.3 is the radius of a circle (nearly) in such parts as the circumference contains 360.

DEFLEXION ANGLE.

To find the deflexion angle corresponding to any given radius. (Chords 100 ft.)

RULE 1.

Divide the chord by the radius; the quotient will be the natural sine of the deflexion angle; therefore, the number of degrees corresponding to this sine, in the table of nat. sines, equals the deflexion angle.

RULE 2.

The deflexion angle may be found by dividing the radius of a 1° curve, 5730, by the radius in feet, (approximately.)

To find the deflexion angle for any plus distance, or less than 100 ft.

RULE 3.

Multiply one-half the deflexion angle by the plus distance, and divide the product by 100 ft. (length of whole chord,) and add it to one-half the deflexion angle.

EXAMPLE.—Suppose we are running a 15° curve by deflexion distances; we wish to find the deflexion angle for 25 ft.

STATEMENT.— $15^\circ \div 2 = 7^\circ 30'$, one-half the deflexion angle.

Then, $7^\circ 30' \times 25 = 187^\circ 30' \div 100 = 1^\circ 52\frac{1}{2}'$.

Then, $1^\circ 52\frac{1}{2}' + 7^\circ 30' = 9^\circ 22\frac{1}{2}'$, deflexion angle for 25 ft.

For deflexion angles corresponding to any given radius, refer to table of radii, page 11.

TANGENTIAL DISTANCE.

To find the tangential distance for any radius, on chords of 100 ft.

RULE 1.

Divide the square of half the chord (50 ft.) by the radius, and multiply the quotient by two.

RULE 2.

Divide the square of the whole chord by twice the radius.

To find the tangential distance for any number of feet less than 100.

RULE 3.

Multiply the tangential distance for 100 ft. by the number of feet required, less than 100 ft., and divide the product by 100 ft., and from the quotient take the ordinate corresponding to the degree of curvature and feet; will equal the tangential distance for the required number of feet, less than 100 ft.

To find the tangential distance for any number of feet.

RULE 4.

Divide the square of the chord given by twice the radius.

In running curves, with equal chords on more than 100 ft., the tangential distances increase as the squares of the number of chords: thus, for 2, 3, 4, 5, 6 chords, 4, 9, 16, 25, 36, multiplied into the tangential distance of 1 chord, will equal each tangential distance respectively.

Or: the square of the length of the chord divided by twice the radius, will equal the tangential distance for any number of feet.

TABLE OF TANGENTIAL DISTANCES.

Deflexion Angle.	Length of Chords in Feet.			
	100	75	50	25
0				
30	0.436	0.245	0.109	0.027
45	0.654	0.367	0.164	0.040
1	0.873	0.490	0.218	0.054
30	1.309	0.736	0.327	0.081
45	1.527	0.858	0.381	0.095
2	1.745	0.981	0.436	0.109
30	2.182	1.227	0.546	0.136
45	2.399	1.349	0.599	0.150
3	2.618	1.472	0.655	0.163
30	3.054	1.717	0.763	0.190
45	3.272	1.841	0.818	0.205
4	3.490	1.963	0.872	0.218
30	3.927	2.209	0.982	0.246
45	4.145	2.331	1.036	0.259
5	4.361	2.452	1.089	0.272
30	4.798	2.698	1.199	0.299
45	5.015	2.820	1.252	0.312
6	5.235	2.944	1.308	0.326
7	6.105	3.432	1.524	0.380
8	6.975	3.924	1.741	0.433
9	7.840	4.406	1.955	0.486
10	8.715	4.899	2.174	0.541
11	9.585	5.387	2.391	0.594
12	10.470	5.885	2.615	0.650
13	11.340	6.373	2.831	0.703
14	12.210	6.860	3.047	0.755
15	13.080	7.348	3.263	0.808

TANGENTIAL ANGLES.

To find the tangential angle for a chord of 100 ft., with any given radius.

RULE 1.

Divide half the chord by the radius; the quotient will be the natural sine of the tangential angle; and the angle corresponding to this sine, in the table of nat. sines, is the angle required.

To find the tangential angle for any number of feet less than 100 ft.

RULE 2.

Multiply the tangential angle by the number of feet given, and divide the product by the length of the whole chord, (100 ft.)

EXAMPLE.—Suppose we have the tangential angle $= 7^{\circ} 30'$, and wish to find the angle for 25 ft.

STATEMENT.— $7^{\circ} 30' \times 25 \text{ ft.} \div 100 \text{ ft.} = 1^{\circ} 52\frac{1}{2}'$, tangential angle for 25 ft.

Sometimes in running curves it is not necessary to set points in every chord, or 100 ft., and is more expedient, as running curves on a preliminary survey. They can be put in every 2, 3, or 400 ft., as you choose. We wish to find the tangential angle for any number of chords.

RULE 3.

Multiply the tangential angle for 100 ft. by the number of chords you wish to subtend, will equal the tangential angle required.

REMARK.—In running curves, the correct way of measuring with a chain for each station, is to measure around the curve. Instead of this the chain is stretched across, forming a chord; the difference of distance is so comparatively small to a radii of 500 ft., that it is not necessary we should measure around, or make an allowance on the chain; but in running curves with long chords of 3, 4, or 500 ft., it is necessary, for accuracy, to make sufficient allowance, for which I will put in a table of long chords the lengths necessary to subtend from 1 to 4 stations.

TABLE OF LONG CHORDS.

Deflexion Angle.	Length of Chords in Feet required to Subtend.			
	1 Station.	2 Stations.	3 Stations.	4 Stations.
0				
1	100	200	300	400
2	100	200	299.9	399.7
3	100	200	299.7	399.3
4	100	199.9	299.6	398.9
5	100	199.9	299.2	398.0
6	100	199.7	298.8	397.3
7	100	199.6	298.4	396.2
8	100	199.6	298.0	395.1
9	100	199.4	297.5	394.1
10	100	199.2	297.0	392.4

To find the length of long chords.

RULE 4.

Multiply the natural sine of the tangential angle of the given chord by twice the radius.

EXAMPLE.—The tangential angle for one station = 5° , and radius = 573.7 ft; what would be the length of the chord of four stations?

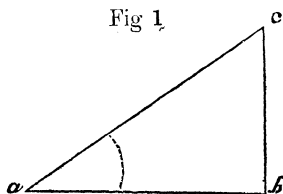
STATEMENT.—The tangential angle for four stations would equal $4 \times 5^\circ = 20^\circ$, and nat. sine of $20^\circ = .3420201$; twice the radius $= 1147.4 \times .3420201 = 392.4$, length of chord necessary to subtend an arc of four stations.

TRIGONOMETRY.

The angle a given, (Fig. 1) and hypotenuse given, to find the leg $c b$.

RULE 1.

By natural sines.—As unity, or one, is to the length of the hypotenuse, so is the natural sine of the smallest angle to the length of the shortest leg.



EXAMPLE.—Given the angle $b a c$ $35^\circ 30'$, and hypotenuse 25 rods; to find $c b$.

STATEMENT.— $1 : 25 :: 0.580703 : 14.5175$.

To find the length of the leg $a b$.

RULE 2.

The difference of the sums of the squares of the legs $a c$ and $c b$, and extract the square root; will equal the leg $a b$.

EXAMPLE.—Given the leg $a c$ 25 rods, and leg $c b$ 14·5175; to find the leg $a b$.

STATEMENT.— $\sqrt{25^2 - 14\cdot5175^2} = 20\cdot35$.

To find the leg $a b$, (Fig. 1.)

RULE 3.

By nat. sines.—As unity, or one, is to the nat. sine of the angle $a c b$, so is the hypotenuse to the leg $a b$.

EXAMPLE.—Given the hypotenuse 25 rods, and angle $a c b$ $54^\circ 30'$; to find the leg $a b$.

STATEMENT.— $1:0\cdot8141155::25:20\cdot35$.

The angles and leg $a b$ given, (Fig. 1) to find the hypotenuse $a c$, and leg $b c$.

RULE 4.

By nat. sines.—As the nat. sine of the angle opposite the given leg $a b$ is to the length of given leg, so is unity, or one, to the length of the hypotenuse.

EXAMPLE.—Given the angles $a c b$ $54^\circ 30'$, and $b a c$ $35^\circ 30'$, and leg $a b$ $20\frac{35}{100}$ rods; to find the leg $a c$.

STATEMENT.— $0\cdot8141155:20\cdot35::1:25$.

Refer to Rule 2, page 38.

To find leg $c b$ by nat. sines.

RULE 5.

As the nat. sine of the angle $a c b$, opposite the given leg, is to the given leg, so is the nat. sine of the angle $b a c$, opposite the required leg; to the leg $c b$.

EXAMPLE.—Given the angle $a c b$ (Fig. 1) $54^{\circ} 30'$, and angle $b a c$ $35^{\circ} 30'$, and leg $a b$ $20\frac{35}{100}$ rods; to find the leg $b c$.

STATEMENT.— $0.8141155:20.35::0.580703:14.52$, leg $b c$.

The hypotenuse and one leg given; to find the angles and the other leg.

RULE 6.

By nat. sines.—The angle opposite the given leg may be found by the following proportion: As the hypotenuse is to unity, or one, so is the given leg to the nat. sine of its opposite angle.

EXAMPLE.—Given the hypotenuse $a c$ 25 rods, and leg $a b$ 20.35 rods; to find the angles.

STATEMENT.— $25:1::20.35:0.8141155$, nat. sine of the angle $a c b$; the nearest corresponding number of degrees and minutes in the table of nat. sines gives the angle $a c b$ $54^{\circ} 30'$, and the angle $a b c$ being 90° , the angle $b a c$ would be $35^{\circ} 30'$, because in a right-angle triangle there is always 180° .

The leg $a c$ given, (Fig. 1) and angle $b a c$, to find the other leg, $a b$, by cosine.

RULE 7.

Multiply the cosine of the angle $b a c$ by the hypotenuse $a c$.

EXAMPLE.—Given the hypotenuse $a c$ 25 rods, and angle $b a c$ $35^{\circ} 30'$; to find the leg $a b$.

STATEMENT.— $0.8141155 \times 25 = 20.35$, length of the leg $a b$.

The leg $a b$ found, (Fig. 1) to find the leg $b c$ by nat. tangent.

RULE 8.

Multiply the base by the nat. tangent of the angle opposite the required leg.

EXAMPLE.—Given the leg $a b$ 20.35, and angle $b a c$ $35^{\circ} 30'$; to find the leg $b c$.

STATEMENT.— $0.713293 \times 20.35 = 14.5$, the required leg $b c$.

The angle $a c b$, and leg $b c$, given, (Fig. 1) to find the leg $a b$, by nat. tangents.

RULE 9.

Multiply the nat. tangent of the angle $a c b$ by the leg $b c$.

EXAMPLE.—Given the leg $b c$ 14.5, and angle $a c b$ $54^{\circ} 30'$; to find the leg $a b$.

STATEMENT.— $1.401948 \times 14.5 = 20.35$, length of leg required, $a b$.

Solution of a Right-angled Triangle.

The sine of the angle c equals the cosine of the angle a , and the sine of the angle a equals the cosine of the angle c .

The tangent of the angle a equals the cotangent

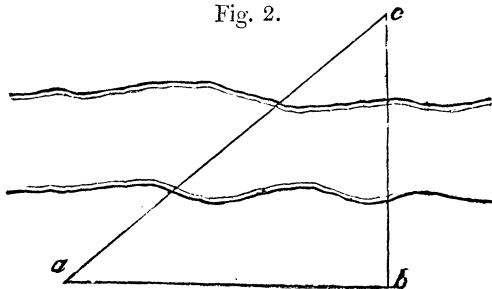
of the angle c , and the tangent of the angle c equals the cotangent of the angle a .

The leg $a b$ divided by the leg $a c$ equals the nat. sine of the angle $a c b$, or the nat. cosine of the angle $b a c$; the leg $b c$ divided by the leg $a b$ equals the nat. tangent of the angle $b a c$, or the nat. cotangent of the angle $a c b$; the leg $b c$ divided by the leg $a c$ equals the nat. sine of the angle $b a c$, or the nat. cosine of the angle $a c b$.

SURVEYING.

In running lines, obstructions, viz: rivers, ponds, &c., occur, by which other means have to be resorted to, besides measuring with a chain.

Fig. 2.

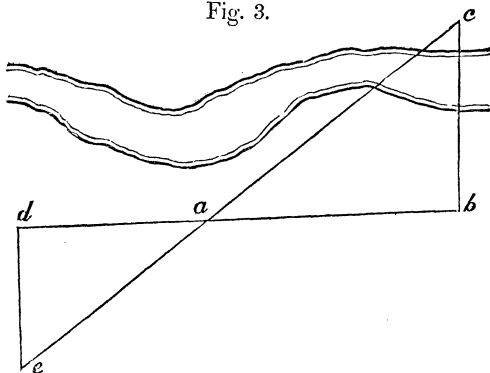


The point c occurs on our line $b c$, and we wish to know the distance $b c$.

RULE 10.

From b at right angles to the line $b c$ measure any convenient distance, as a , and secure the point a ; measure the angle $b a c$; then multiply the nat tangent of the angle $b a c$ by the distance $a b$; will equal the distance $b c$.

Fig. 3.



In case you should not have a book of tables of nat. tangents, the above method could be resorted to, with nearly as much accuracy as the method given in Fig. 2.

The point c occurring in the line, (Fig. 3) we wish to know the distance $b c$.

RULE 11.

At right angles from $b c$ measure on the line $b d$ to a , and secure the point a , any convenient point, and measure any convenient distance, as d , and at

right angles describe the line $d e$, with your instrument at a , on the line $a c$, produce it to e , intersecting the line $d e$.

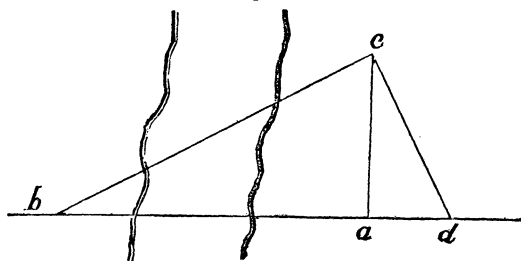
Then with the distance $b a$, $a d$, and $d e$, given, the distance $b c$ can be found proportionately to the triangle $a d e$.

Say: As the distance $a d$ is to $a b$, so is $d e$ to $b c$.

EXAMPLE.—Given the distance $b a$ 20 ft., distance $a d$ 15 ft., and distance $d e$ $11\frac{1}{2}$ ft.; to find the distance $b c$.

STATEMENT.—As $15:20::11\frac{1}{2}:15\frac{3}{10}$ ft.

Fig. 4.



The above (Fig. 4) could be resorted to in preference to Fig. 3.

Given b , the inaccessible object, and $d b$ part of the line of survey; we wish to find the distance from a to b .

RULE 12.

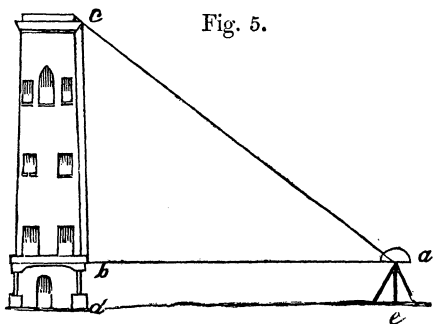
Measure on the line $a c$ (at right angles with $a b$,) any convenient distance, as at c ; then at right angles

to $b c$ run the line $c d$ to its intersection with the line $d b$ at d , measure the distance $a d$, and the distance $a c$.

Then say: The square of $a c$ divided by $a d$ equals $a b$, the distance required.

EXAMPLE.—Given $a c$ 26 ft., and $a d$ $13\frac{1}{2}$ ft.; required the distance $a b$.

STATEMENT.— $26^2 \div 13\frac{1}{2} = 50$ ft., distance $a b$.



We wish to find the height of a tower, or building, as $d c$.

Set your instrument any convenient distance, e , neither too great nor too small, in comparison to the altitude $d c$, and measure the angle $b a c$, and measure the distance $a b$ or $e d$; you then have, in the right-angle triangle, one side given, and the angle $b a c$.

RULE 18.

Multiply the nat. tangent of the angle $b a c$ by the distance $a b$; will equal $b c$.

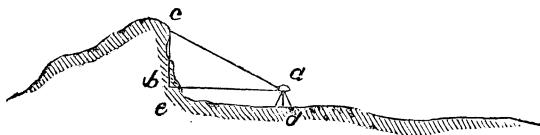
NOTE.—The point at b can be observed, and afterwards the distance $b d$ can be measured, which, added to $b c$, will determine the distance $c d$.

In finding the height of an object, let the observed angle be as near 45° as possible; for then a small error committed in taking it, makes the least error in the computed height of the object; because, if the observed angle, as at a , equals 45° , the distance $a b$ will equal $b c$.

It very seldom occurs, in the construction of a railroad, to measure verticle heights with an instrument.

In running levels, if the top of a hill is found inaccessible to find the elevation with a leveling instrument, we have to resort to the examples given by triangulation.

Fig. 6



When it is necessary to determine the elevation of a hill as in Fig. 6, the elevation at d , is found with the leveling instrument, as will be explained in the Art of Leveling.

EXAMPLE.—Set your instrument over d , and measure the angle $b a c$, and distance $a b$; you then have for the triangle $b a c$, the angle and one leg given,

to find the other leg, $b\ c$, as in Fig. 5; which, added to the height of your instrument, a from d , will equal $e\ c$; and added to your elevation d , will equal the elevation c .

THE ART OF LEVELING.

The first thing necessary in leveling, is to have the requisite instruments in adjustment.

To Adjust a Level.

In the common Y level there are three adjustments.

1st ADJUSTMENT.—Place the instrument in a firm position, and unclamp the Y's; place the horizontal hairs on some distant object, and revolve the telescope half around; if the hair intersects the point first observed, the instrument is in adjustment, thus far; if not, move the hairs half way distant, between the two points of intersection, by means of the screws on the telescope, generally marked "Hairs," and by revolving the telescope, the hairs will intersect our given point. The vertical hairs can be adjusted the same way.

2d ADJUSTMENT.—With the instrument firm, as before.—Fasten the telescope over the leveling screws, and level it exact; then take the telescope out of the Y's and reverse it; if the bubble is level, this adjustment is correct; if not, divide the difference of the

bubble (one-half,) by means of the screws under the bubble, and level the remainder by means of the leveling screws. This process for the second adjustment hardly ever proves correct the first time; therefore, repeat the above, until the telescope, when revolved in the Y's, on every screw, the bubble will be level.

3d ADJUSTMENT.—After the above adjustments, fasten the telescope on the Y's, by means of pins generally used; place your telescope over the leveling screws, and bring the bubble to a level, and repeat it on all the screws, so as to get the telescope as level as possible before commencing the adjustment; then placing the telescope over any two of the leveling screws, and level the bubble; reverse the telescope half way on the pivot, or, as near as possible over the same screws; if the bubble is level, the adjustment is correct, if not, move the bubble half way, by means of the screws under the leg of the Y, and level the remainder by means of the leveling screws. By continuing this process on all the screws, the adjustment can be perfected.

NOTE.—The last adjustment is immaterial, only in saving time and trouble when using. The difference (if there is any,) is so comparatively small, that it is not observable.

The third adjustment never will remain in adjustment on most of levels, so that no trouble need be borrowed when it is found that your level will not reverse correctly. The adjustment of the level now being complete, we will proceed to its use.

In preliminary surveys, or location of railroads,

levels have to be run (as it is termed) to ascertain the exact surface of the ground, in order to establish grades. In commencing levels, an elevation is established upon a given point. This point is generally made by cutting on the root of a tree and is termed a "Bench." These benches are established on the entire length of the line, perhaps one-half to three-quarters of a mile apart, for reference points.

This elevation is generally estimated above, so as to reach the lowest point of the surface of the ground that should occur in your levels. For instance: The lowest point of ground we guess to be 50 ft. below the first established bench, and for safety would call the bench elevation 60. We set up our level firm in the ground, not to exceed 400 ft. from the bench, and near the line we wish to run the levels over, and take what is termed a back sight (marked B. S.) on the bench, by holding the staff, or leveling rod, on the bench, and moving the target of the rod to its intersection with the horizontal hairs in the telescope; what the rod would read at this intersection, would show that our instrument would be that number of feet and parts above the bench. For instance: Suppose the rod read $3\frac{416}{1000}$ ft., therefore, the elevation of the instrument would be 63.416.

When we have the height of the instrument given, it shows very plainly that if you take a sight at any given point, the elevation would be as much less as the rod would read. For instance: Suppose the rod at any point, or station, (as stations of 100 ft. are used in the location of railroad lines,) should read $10\frac{193}{1000}$, which are termed fore, or intermediate sight,

(marked F. S.) the elevation of that point taken would be 53.218 ; or, $63.416 - 10.198 = 53.218$; consequently, these fore sights should be subtracted from the height of the instrument, or elevation of the instrument, to give the elevation of stations.* In order to keep up the same corresponding elevations, on the entire length of the line, we change our instrument on some substantial point, as a peg or stone, by holding the rod upon the peg; being a fore sight, we subtract it from the height of the instrument, which gives the elevation of the peg, and is the same as a bench. Suppose the rod reads on the peg 8.747 , and instrument is 63.416 ; $63.416 - 8.747 = 54.669$, elevation of peg.†

We have the elevation of the peg, and can move our instrument further on, and set up our instrument firm in the ground, as before, and take a "back sight" on the peg, by holding the rod upon the peg, and notice the reading as before. Suppose the rod to read 1.201 ; it shows that our instrument is 1 foot and $\frac{2.01}{1000}$ above the peg; consequently, if we add it to the elevation of the instrument, thus: peg = 54.669 , rod reads $1.201 + 54.669 = 55.870$, height of instrument, and proceed as before, taking intermediate sights, subtracting every intermediate from the

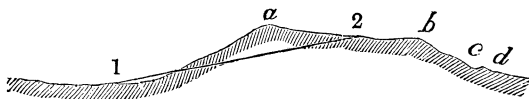
* These fore sights are more properly termed intermediate sights (marked I. S.) which we will hereafter term them, and fore sights will be termed as at changes of the instrument, after running the level of intermediates, not to exceed 400 ft. on either side of your instrument.

† In practice, whether you change your instrument upon a peg, stone, stump, or anything suitable, it is termed a peg.

height of the instrument. It is not necessary to carry out the reading of the rod of the decimals, (when taking intermediates,) farther than hundredths, as 2·27, 4·15, 8·11, &c., and in most cases tenths is far enough, as 2·2, 4·1, 8·1, &c., &c.

Intermediates, or plus stations, should be taken when the ground varies to any amount; discretion on your own part must govern that. It is evident that if you were running levels over an uneven ground, as Fig. 1, and should take the elevation at station 1 and station 2, that you lose, or there would be a loss in the estimate of the quantities, or if for the purpose of establishing grades, a correct line could not be drawn, as a man's discretion is governed by the correctness of the profile, or levels taken, therefore, a level should be taken at *a*, also at *b c d*, and the plus station noted in the book of levels, then you have the correct shape of the ground.

Fig. 1.



To explain the foregoing more intelligibly, we will refer to Figs. 2, 3, and 4.

Our established bench elevation 60, is at *A*, on the root of a stump; our line to run is in the direction of *d*, consequently, we would set our level at *c*, not to exceed 400 ft. from the bench *A*; in directing our level at the target *f*, we find it reads 3·416; then

our level would be that number of feet and parts above the point *a*; bench elevation is 60, elevation of instrument would be $60 + 3.416 = 63.416$; we will take the elevation of the ground at the stations 1, 2, 3, 4, 5, 6, &c., reading Fig. 2.

the nearest tenth of a foot, on the rod.

Station 1 reads 3.5, therefore, $63.416 - 3.5 = 59.916$, or 59.9

elevation of station 1.

Station 2 reads 3.3, then $63.4 - 3.3 = 60.1$.

Station 3 reads 3.6, then $63.4 - 3.6 = 59.8$.

Station 4 reads 3.7, then $63.4 - 3.7 = 59.7$.

Station 5 reads 3.6, then $63.4 - 3.6 = 59.8$.

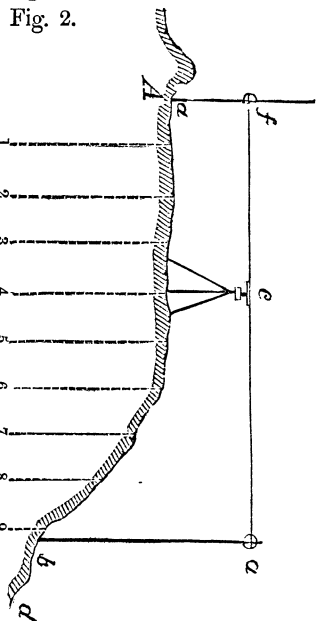
Station 6 reads 3.9, then $63.4 - 3.9 = 59.5$.

Station 7 reads 4.8, then $63.4 - 4.8 = 58.6$.

Station 8 reads 5.8, then $63.4 - 5.8 = 57.6$.

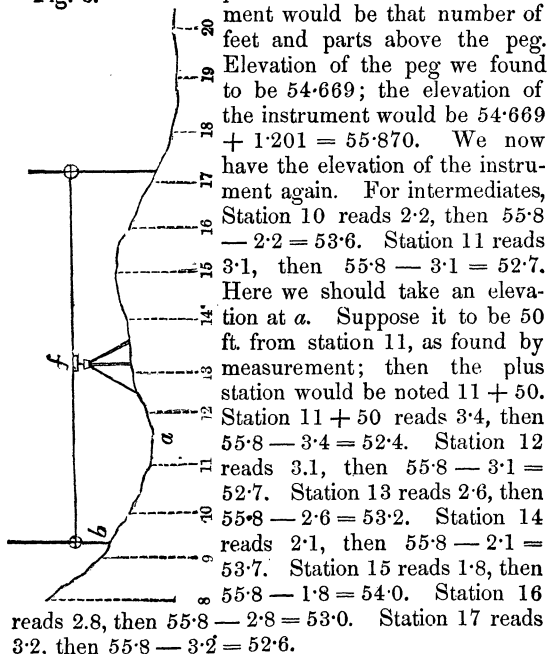
Station 9 reads 8.4, then $63.4 - 8.4 = 55.0$.

We will change our instrument at station 9, for convenience. We drive in a peg, firm into the ground, at or near the station; the rod reads 8.747,



then $63.416 - 8.747 = 54.669$, elevation of the peg at *b*. This being a secured point, we move our instrument, as in Fig. 3, to *f*. After firmly setting our instrument, we take a back sight on the peg *b*. Suppose

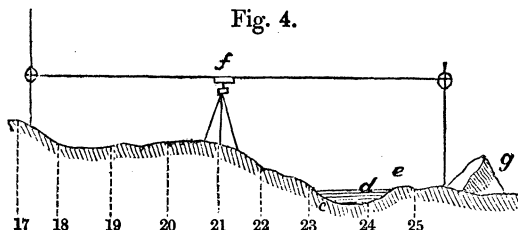
Fig. 3.



We will change our instrument by driving a peg

at or near station 17, and finding its elevation.* Suppose the F. S. on the peg reads 3.775, then height instrument $55.870 - 3.775 = 52.095 =$ elevation of peg; we then move our instrument to *f*, (Fig. 4) and take a B. S. on the peg. Suppose it to read 2.000; elevation peg $52.095 + 2.000 = 54.095 =$ height of instrument. Then proceed as before.

Fig. 4.



Station 18 reads 3.0, then $54.1 - 3.0 = 51.1$.

Station 19 reads 2.9, then $54.1 - 2.9 = 51.2$.

Station 20 reads 2.7, then $54.1 - 2.7 = 51.4$.

Station 21 reads 2.5, then $54.1 - 2.5 = 51.6$.

Station 22 reads 3.6, then $54.1 - 3.6 = 50.5$.

Station 23 reads 4.4, then $54.1 - 4.4 = 49.7$.

Here at station 23 we have come to a stream, and it is quite necessary to get its shape, width, and character. We have got the elevation of the top of the slope of the river at station 23; we take an elevation at *c*, at the bottom of the slope of the creek, and notice its plus distance from station 23. Suppose it to be 25 ft.; then $23 + 25$ would be the bottom

* When changing, the elevations should be exact.

slope of the stream. We also get the elevation of the bottom of the slope on the opposite side *d*, and notice the plus station. Suppose it to be 85 ft. from station 23, then it would be $23 + 85$, bottom slope of stream; and station 24 would also be taken, as we very seldom miss stations, wherever they may occur. We have the top slope 23, and two bottom slopes $23 + 25$, and $23 + 85$, and to complete the levels of the creek we want the top slope of opposite side. Say it is 75 ft. from station 24; then elevation at $24 + 75$ gives the shape of the river's banks and bottom. Also to govern the masonry, or bridging, over this stream, the elevation of high water mark is taken. This will be readily found by inquiry, if no signs on the banks are visible.

Other very important things have to be observed and placed under remarks, which your own discretion must lead you.

We will establish a bench before proceeding farther. Say, for instance, we cut a notch on the root of the stump *g*. Suppose our rod, or F. S., reads 4.005; height of instrument 54.095 — 4.005 = 50.090, elevation of the bench. The elevation of the benches are generally marked on the stump with either red chalk or paint. We secure this elevation at *g*, and along the line at intervals, to avoid the trouble of going back to the first established bench, *A*, Fig. 2, on the line. For instance: Suppose it is required to find the elevation of station 25, or wished to stake out a bridge, or stone culvert, in the stream at some future day. We, instead of running from the first established bench, take the established bench *g*, by

setting our instrument say at *f*, the most convenient point, and do the work required.

We proceed with our levels as before, and establish benches, or elevations, not to exceed three-quarters of a mile apart.

It might be necessary to state, for accuracy in running levels, that the rod should be plumb, or point to the centre of the earth; also the bubble of the level should always be level. Accuracy depends both upon the leveler and rodman.

I will here give the manner of keeping a field-book for running levels.

NOTE.—In running levels, always add the back sights, which will give the elevation of the instrument, and subtract the fore or intermediate sights, will give the elevation of the peg or bench.

MANNER OF KEEPING FIELD-BOOK.

NOTES FROM FORMER EXAMPLES.

Sta'n.	B. S.	F. S.	I. S.	H. Inst.	Elev' n.	Remarks.
B'ch	3·416			63·416	60·000	On root of stump near stat'n 1.
1			3·5		59·9	
2			3·3		60·1	
3			3·6		59·8	
4			3·7		59·7	
5			3·6		59·8	
6			3·9		59·5	
7			4·8		58·6	
8			5·8		57·6	
9			8·4		55·0	
Peg.		8·747			54·669	Elevat'n of peg at B. (Fig. 2.)
10	1·201		2·2	55·870	53·6	
11			3·1		52·7	
+50			3·4		52·4	

Stat'n.	B. S.	F. S.	I. S.	H. Inst.	Elevat'n.	Remarks.
12			3.1	63.416	52.7	
13			2.6		53.2	
14			2.1		53.7	
15			1.8		54.0	
16			2.8		53.0	
17			3.2		52.6	
Peg.		3.775			52.095	
18	2.000		3.0	54.095	51.1	
19			2.9		51.2	
20			2.7		51.4	
21			2.5		51.6	
22			3.6		50.5	
23			4.4		49.7	Top of bank of stream.
+25			5.2		48.9	Bottom of stream.
+85			5.3		48.8	Bot. of stream, opposite side.
24			5.0		49.1	
+75			4.4		49.7	Top slope of opposite side.
			4.6		49.5	High water mark.
B'ch		4.005			50.090	On stump by station 26.

In leaving the work at night, benches should be made, so that when you choose at any time to go to work, you have a convenient place to commence, and accurate.

After the levels are run the work is plotted and grades are established.

Grades vary in their ascent according to circumstances, and are governed by the discretion of the engineer in charge. They intend however to equalize the excavation and embankment as near as possible. Grades sometimes can be improved, and are governed by the contracts taken to grade the road.

Grades have elevations as well as the surface of the ground. We will assume the grade at Station

tablished, and construction commences. We then have different field books, termed Grade Book, Cross Section Book and Monthly Estimate Book.

MANNER OF KEEPING GRADE BOOK.

Sta'n.	Grade.	Cut.	Fill.	Elev'n	Remarks.
1	58.000	1.9		59.9	
2	57.780	2.3		60.1	
3	57.560	2.2		59.8	
4	57.340	2.4		59.7	
5	57.120	2.7		59.8	
6	56.900	2.6		59.5	
7	56.680	1.9		58.6	
8	56.460	1.2		57.6	
9	56.240		1.2	55.0	
10	56.020		2.4	53.6	
11	55.800		3.1	52.7	
+50	55.690		3.3	52.4	
12	55.580		2.8	52.7	
13	55.360		2.1	53.2	
14	55.140		1.4	53.7	
15	54.920		0.9	54.0	
16	54.700		1.7	53.0	
17	54.480		1.8	52.6	
18	54.260		3.1	51.1	
19	54.040		2.8	51.2	
20	53.820		2.4	51.4	
21	53.600		2.0	51.6	
22	53.380		2.9	50.5	
23	53.160		3.4	49.7	Top of bank of stream.
+25	53.105		4.2	48.9	Bottom of stream.
+55	52.973		4.1	48.8	Bottom of stream opposite side.
24	52.940		3.8	49.1	
+75	52.775		3.0	49.7	Top of slope opposite side.

The benches are all entered in the back part of the grade book for reference when necessary. In

the grade book we have the cuts and fills worked out, but in the staking out of the work, these cuts and fills are merely used for tests. Engineers generally have in all their work test points for reference, which all should have, to avoid the many mistakes that will occur.

In staking out work the grade point or where the excavation and embankment commences, is always found with its distance from the station joining, and a stake put in to guide the contractors in commencing their work.

The grade points are generally marked in the cross section book.*

Cross sections are cuts and fills taken at right angles to the line of the road, any distance from the center line that should seem necessary by the engineer.

Cross sections are taken with the level, but more plus stations are taken, than in running levels, as the discretion of the engineer may direct him. Cross sections are taken to get as near as possible the amount of cubic yards excavation and embankment, as contracts are taken of the work, to complete at a given price per cubic yard. On very level ground, cross sections are taken at every station. On very uneven ground cross sections are taken as often as your judgment dictates.

Before proceeding further, we will explain the manner of getting the cuts and fills with a level in the field.

*This cross section book is more properly termed Original Cross Section Book, as there also is the Final Cross Section Book.

With the grade book we have the elevation of grade. We go into the field, say at station 21, and set up our level, and take a B. S. on the bench *g*, (Fig. 4,) and find the elevation of our instrument. Suppose the elevation of the bench to be 50.090, and rod reads 5.112, then $50.090 + 5.112 = 55.202$, elevation of instrument. Suppose we wish to commence at station 19, with our cross sections. We would refer to the grade book at station 19 and find the elevation of grade at that point = 54.040. We now have the elevation of our instrument and the elevation of the grade at station 19. Now if we subtract the elevation of the grade from the elevation of the instrument, the difference shows that our instrument is that number of feet and parts above the grade line at station 19. For instance:

$$\begin{aligned} \text{Elevation of instrument} &= 55.202 \\ \text{grade} &= 54.040 \\ \text{Difference of elevation} &= 1.162 \end{aligned}$$

Then our instrument at station 19 is 1.162 feet above the grade line. We will get the cut or fill at station 19. Suppose our rod to read, at station 19, 4.0, (the nearest tenth of a foot,) it would show our instrument to be four feet above the surface of the ground, and if our instrument is 1.162, (or nearest tenth,) 1.2 above the grade line, and 4.0 above the surface, we see that if we take their differences, it will give the fill or cut at station 19. Then—

$$\begin{aligned} \text{Elevation of instrument above surface of ground} &= 4.0 \\ \text{grade} &= 1.2 \\ \text{Difference} &= 2.8 \end{aligned}$$

2.8 is then the fill at station 19. We then take our cross section at station 19, subtracting the height of instrument above the grade line, 1.2, from the height of the instrument above the surface, will equal the cut or fill at station 19, any distance at right angles from the station or center line.

We see that our instrument at station 20 (by reference to a profile) would not be 1.162 above the grade line, but would be more as the grade descends. We have found that the grade descends $0.22\frac{2}{100}$ per 100 feet. Then if we add 0.22 to the instrument above the grade line at station 19, will equal its height above the grade line at station 20. Then elevation of instrument at station 19 = 1.162; descends 0.22 per 100 feet, or station, then $0.22 + 1.162 = 1.382$; height above station 20 = 1.382.

We will suppose the rod reads at station 20, 4.0, the same as station 19, then $4.0 - 1.4$ (nearest tenth of 1.38) = 2.6 fill, or 2 feet and 6 tenth is the difference between the grade line and the surface of the ground at station 20.

We can continue this process to all the stations, until it becomes necessary to change the instrument. When we change, the elevation of the instrument we have preserved = 55.202, and change on a peg, as in running levels, subtracting the sight on the peg for its elevation, and after the instrument is set up again, add the sight to the elevation of the peg, and you have the height of your instrument again, and proceed as you commenced.

Sometimes we find our instrument below the grade line. We will suppose that the rod reads on the

bench *g*, (Fig. 4,) 2.950; this added to the bench would give the elevation of the instrument; bench = $50.090 + 2.950 = 53.040$, height of instrument. Grade at station 19 = 54.040. Now we have the elevation of the instrument, less than the elevation of the grade—

Thus, elevation of instrument = 53.040

“ grade at stat. 19 = 54.040

Difference of elevation = 1.000

Shows that our instrument is 1 foot below the grade line. Now if our instrument is below grade, the sights on the surface must be added to the elevation of the instrument, to give the difference or distances of the grade line to the surface. Suppose the rod, or sight, at station 19, reads 1.8. We would see that the surface of ground was 1 foot and 8 tenths below the instrument, and the instrument is 1 foot below the grade line, therefore the distance from the grade line to the surface of the ground, would be their sum. Thus,

Elevation of instrument below grade = 1.00

“ “ above surface = 1.8

Difference of surface and grade line = 2.8

2.8 would be the fill at station 19.

When you come to grade, the elevation of the instrument above the grade line, and its elevation above the surface of the ground, will be equal.

For example, suppose the instrument be 1.2 above the grade line, and surface of the ground 1.2, the difference is 00, and is the point of grade.

If the elevation of the surface and elevation of grade are equal at any point, that part of the surface

of the ground is grade, or the point where the excavation and embankment commences. Thus,

$$\begin{aligned}\text{Elevation of grade} &= 54.040 \\ \text{Elevation of surface of ground} &= 54.040 \\ \text{Difference} &= 0.00\end{aligned}$$

In taking cross sections, the elevation of the instrument should be preserved for changing — and to be correct, you should keep a table of both your elevation of peg and instrument and height of instrument above the grade line at each and every station. To show more plainly, we will make a sketch of the work already done:

$$\begin{aligned}\text{Bench} &= 50.090 \\ \text{B. S.} &= \underline{5.112} \\ \text{H. Inst.} &= 55.202 \\ \text{Change Inst., F. S.} &= \underline{2.211} \\ \text{Peg} &= 52.991 \\ \text{B. S.} &= \underline{0.049} \\ \text{H. Inst.} &= 53.040\end{aligned}$$

$$\begin{aligned}\text{Also,— Grade at stat. 19} &= 54.040 \\ \text{H. Inst.} &= \underline{55.202}\end{aligned}$$

$$\begin{aligned}\text{H. Inst. at stat. 19, above grade line} &= 1.162 + \\ \text{Grade descends 0.22 per 100 feet} &= \underline{0.22}\end{aligned}$$

$$\begin{aligned}\text{H. Inst. at stat. 20, above grade line} &= 1.382 + \\ &= \underline{0.22}\end{aligned}$$

$$\begin{aligned}\text{H. Inst. at stat. 21, above grade line} &= 1.602 + \\ &= \underline{0.22}\end{aligned}$$

$$\begin{aligned}\text{H. Inst. at sta. 22, above grade line} &= 1.822 + \\ \text{\&c., \&c. Change instrument.}\end{aligned}$$

We have the height of instrument again, 53·040, and will commence at station 19 again to show the manner of keeping notes with the instrument below grade:

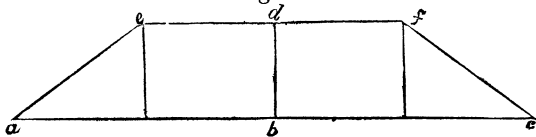
Grade at stat. 19 =	54·040
H. Inst. =	<u>53·040</u>
H. Inst. at sta. 19 =	1·000—
“ “ 20 =	0·780—
“ “ 21 =	0·560—
“ “ 22 =	0·340—

The sign of plus and minus can be annexed to the above, to show that the instrument is above or below grade line. Thus, + = above, — below.

In running from station 19 down the grade, we notice that we add the descent, per 100 feet, to the height of the instrument when plus, and when minus we subtract, because when the instrument is above, the further we run on the descent the greater the height of the instrument from the grade line, as much greater as the descent per 100 feet; and when the instrument is minus, we subtract the descent, because we near the grade line every 100 feet, as the descent of the grade per 100 feet.

Sometimes, in staking out work, it is not necessary

Fig. 5.



to cross section further than where the slope stakes would occur, as in Fig. 5.

The above shows a cross section, $a b c$, with the slopes $a e f c$, determined, and slope stakes $a c$ put in.

The slope of a railroad is governed by the material of which it is composed.

The excavations are governed the same as the slopes of embankments; the width at the top is governed by the width of track or material. We will assume it to be 14 feet.

In making a cross section of the above, we will assume slopes of $1\frac{1}{2}$ feet horizontal to one foot vertical, as the required slopes. Suppose we take a level at b , (surface of the ground and center of the road,) and find the fill to be four feet. We mark the stake b with red chalk, "4 feet fill," (this is to guide the contractor,) and measure out from b , on either side towards a , one-half the width of the road bed, 7 feet, and take the cutting or filling. From this filling, we can judge of the point for a slope stake a , if the ground does not vary too much; if it should, we keep trying until the exact point for the slope stake is found. For example, we take the level at a , and find that there is $3\frac{3}{10}$ feet filling, and, by calculation, slopes $1\frac{1}{2}$ to 1, we measure from the center 7 feet, and base of slope $5\frac{7}{10}$, making in all to measure from the center line, (as one end of the tape or chain should always be kept at the center stake to avoid confusion in changing from one side to the other,) would equal $12\frac{7}{10}$. We take another sight if it varies much from the point in which we took our sight, and make the same calculations again. It may vary

2 or 3 tenths in the distance from the point last found, but if the ground is level, or nearly so, the required distance can be measured for the slope stake. You go through the same process on the opposite side for the slope stake *c*. We now see that if the contractor fills in 4 feet at *b* to *d*, and 7 feet from *d* to *e*, and 7 feet from *d* to *f*, and carries the dirt out to the slope stakes *a* and *c*, that the slope of the cross sections would have $1\frac{1}{2}$ feet horizontal to 1 foot vertical. Slopes more general in use are $1\frac{1}{2}$ feet horizontal to 1 vertical; 2 feet horizontal to 1 vertical; 1 horizontal to 1 vertical. Calculations for slopes will be found in the following rules:

Slopes $1\frac{1}{2}$ to 1.—With the filling or cutting given, to find the length of the base of the slope.

RULE 1.

One half the cut or fill added to the cut or fill where it is taken.

EXAMPLE.—Given the filling 3·8, to find the base of the slope.

STATEMENT.— $\frac{1}{2}$ of 3·8 = 1·9 + 3·8 = 5·7.

Slope 2 to 1.—With the filling or cutting given as before, to find the base of the slopes.

RULE 2.

Multiply the cutting or filling by 2.

EXAMPLE.—Given the filling 3·8 to find the base of the slope = 3·8 × 2 = 7·6.

Slope 1 to 1—

RULE 3.

The base is equal to the filling or cutting.

EXAMPLE.—Given the filling or cutting 3·8; then the base would equal 3·8.

CROSS SECTIONS.

The number of cross sections to be taken will be as the engineer's judgment governs him, but we will give a few examples necessary to correctness in side hill ground entering from a cut to a fill. The following figures 6, 7 and 8 will represent the cross sections.

In leaving the cut (Fig. 6) a cross section should be taken where the grade point occurs at the bottom slope as at *a*, also a cross section should be taken (Fig. 7) where the grade point occurs at the center *B*; also where the grade point occurs on the opposite side *c*. (Fig. 8.)

Cross sections taken in this manner, give the shape of the ground as near as can be got at. We also have them in plane figures. The area of Fig. 6 to correspond with the area *B c d* (Fig. 7) and *Pyd a B e*, also the *Pyd B c d*, the area *a B e* to correspond with the area *a b c* (Fig. 8). The quantities in this manner are got as correct as is possible. Cross sections around curves should not exceed 50 ft. apart when the average form is used for calculating quantities.

Henck gives a formula for estimating the quantities in curves, but it has been adopted only by a very few engineers, if any. My mode is most in practice

by eminent engineers at present, but there is no doubt that the manner in which Henck and also Trautwine do their work will come into general practice, as the immense quantities of earth that is estimated by the average form would be very materially diminished.

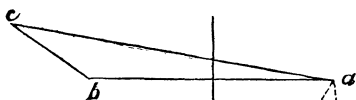


Fig. 6.



Fig. 7.

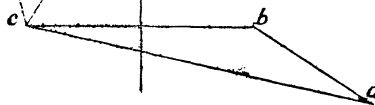


Fig. 8.

BORROWING PITS

Consist of borrowed earth from a hill or side of a mountain, when the earth in the cut is not sufficient for the embankments.

It very often occurs where earth has to be borrowed to finish up embankments; sometimes it is taken from ditches; sometimes knolls are cut off, and sometimes it is taken out of the side of hills and mountains. This amount taken out has to be ascertained in cubic yards.

The Manner of Measuring Borrowing Pits, to ascertain the Quantities taken out.

The object in the first place, is to make original surveys or cross sections; and secondly to make cross sections, (after the earth is taken out) to correspond with the original cross sections. In order to do this, points must be established in the original survey, that can be referred to when you wish to make the second survey. Sometimes it has to be measured monthly, to make monthly estimates.

In order to get correct measurements we will establish a line, (called a Base Line) along the base of the hill* between two points, that will cover the length of the area. For security, the points we will establish upon the roots of some stumps, and in a direct line between these two points, put in stations and plus stations as often as is considered necessary. From these stations, at right angles to the established

* This is governed altogether by the engineer's judgment.

line, measure with the tape or chain, and where it is necessary take sights with the level, and ascertain the elevation, or cut or fill above a certain given point. Continue on this measurement and elevations back as far as will cover the area to be excavated in that direction; continue the same process at every station and plus station. The notes will be entered in the original cross section book.

If it is necessary to make a monthly estimate, the base line is found, and stations and plus stations are put in as before, and measurements are commenced as before. This is entered into the monthly cross section book.

When the work is completed, a final measurement has to be made, by finding the base line, and proceed as in making the original survey.

These elevations are taken with the level. A base line of levels is established for the pit, and when sights are taken, the notes show the elevation of the ground, either above or below the established base line of levels. When the last survey is made, where the earth has been taken out, the difference of elevation at their corresponding points would show the depth of earth taken at these points.

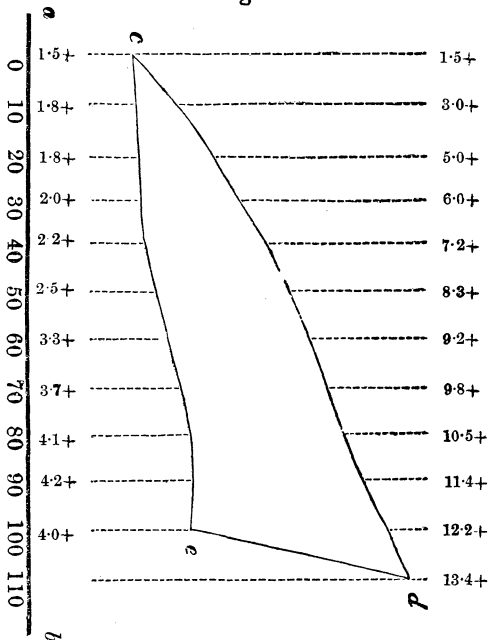
When those measurements are made, they are plotted upon paper, which will show the area of the cross section.

For example, suppose $a b$ (Fig. 9) to be the base line of levels.

The original levels commence at the base line of stations, 1 foot 5 tenths above the base line $a b$, and at the top of the hill, or the extent of excavation, the

elevation is 13 feet 4 tenths above the base line. When the second measurement is made, we find at the station to be the same as the original, 1 foot 5

Fig. 9.



tenths, and find the last point to be 4 feet above the base line. The excavation we find at the top to be

110 feet from the point at *c*, and at the bottom, *e*, or second survey, 100; this will make the slope *d e*, and complete the area *c d e*.

The depth of excavation can be ascertained by the difference of the elevations.

For instance, the depth of cutting 80 feet from the station *c* equals the difference of the elevations 4.1 and 10.5 = 6.4; the cutting then at 80 feet distance is 6 feet 4 tenths. The remainder of the area is ascertained in the same manner. In the notes the sign of + is annexed to the sights when above the base line of levels, and — when below.

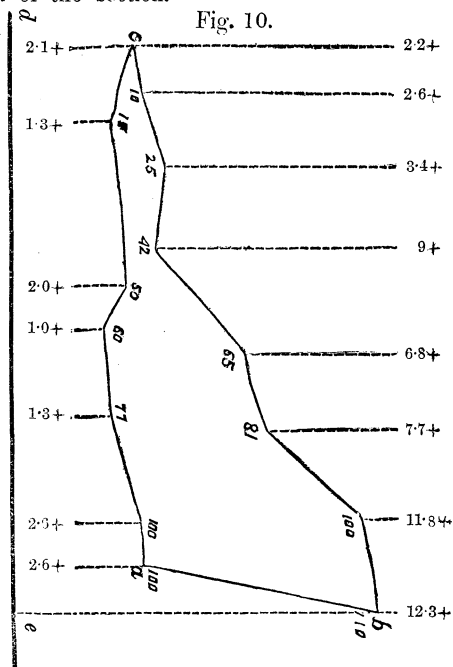
If in two corresponding sights or elevations, one should be below the base line of levels and the other above, the depth of excavations would equal their sum.

If in two corresponding sights or elevations, both should be below the base line of levels, their difference would equal the depth of excavation; if both should be above, their difference would equal the depth of excavations.

NOTE.— All horizontal measurements, with a tape or chain, either in measuring for cross sections or land, should be measured perpendicular to the center of the earth.

The area of the cross sections (Fig. 9) is easily determined, as the original elevations and final elevations correspond in their distance from the station *c*. It is not always that cross sections can be taken with equal distances (10, 20, 30 feet, &c.) from the station, as the ground may be very irregular both in the original and final measurement. The area of the section is ascertained by calculating the area of the

original measurement to the base line of levels, and the area of the final measurement to the base line of levels; the difference of these areas would be the area of the section.



For example, to ascertain the area of section *a b c*, (Fig. 10.)

Instead of the distances 10, 20, 30, &c., from the station at *c*, we have been obliged (on account of the unevenness of ground) to measure the distances 10, 25, 42, 65, 81, 100 and 120 from the station *c*, and in the final the distances 15, 50, 60, 77, 100 and 110. In this case the depth of excavation cannot be ascertained, but the area is easily found.

We wish to get the area of the section *a b c*. By computing the area *b c d e*, and area *b e d c a*, the difference of their areas would equal the area *a b c*.

The manner of keeping original cross section book and final cross section book, is similar. For example, we will arrange Fig. 9 and Fig. 10, supposing that Fig. 9 = stations 1, and Fig. 10 = stations 1 + 20.

ORIGINAL CROSS SECTIONS.

Stations 1.

1.5+	3.0+	5.0+	6.0+	7.2+	8.3+	9.2+	9.8+	10.5+	11.4+	12.2+	13.4+
10	20	30	40	50	60	70	80	90	100	110	

Station 1 + 20.

2.2+	2.6+	3.4+	2.9+	6.8+	7.7+	11.8+	12.3+
10	25	42	65	81	100	120	

FINAL CROSS SECTIONS.

Station 1.

1.5+	1.8+	1.8+	2.1+	2.2+	2.5+	3.3+	3.7+	4.1+	4.2+	4.0+
10	20	30	40	50	60	70	80	90	100	

Station 1 + 20.

2.2+	1.3+	2.0+	1.0+	1.3+	2.6+	2.6+
15	50	60	77	100	110	

When the above is plotted, it forms the figures 9 and 10.

The number of cubic yards contained between

these two figures (according to the present mode of calculation) is equal to one-half the sum of their areas, multiplied by the distance they are apart, (20 feet,) and the quotient divided by 27.

MENSURATION OF SURFACES.

To find the area of a right-angled triangle.

RULE 1.

Multiply one-half the base by the perpendicular height, equal the area.

To find the area of a triangle.

RULE 2.

Multiply the base by the perpendicular let fall on to it from the opposite angle, and one-half the product equals the area.

To find the area of a triangle by its sides.

RULE 3.

From half the sum of the three sides subtract each side separately; then multiply the half sum and the three remainders continually together, and the square root of the product will equal the area.

To find the area of a rectangle or a square.

RULE 4.

Multiply the perpendicular height by the length, equal the area.

To find the area of a rhombus or a rhomboid.

RULE 5.

Multiply the length by the perpendicular distance let fall from its sides, equals the area.

To find the area of a trapezoid.

RULE 6.

Multiply one-half the sum of the parallel sides by the perpendicular, equals area.

To find the area of a trapezium.

RULE 7.

Multiply the diagonal by the sum of the two perpendiculars falling upon it from the opposite angles, and half the product equals area.

To find the area of a regular polygon.

RULE 8.

Multiply one of its sides into half its perpendicular distance from the center, and this product into the number of sides, equals its area.

To find the area of an irregular polygon.

RULE 9.

Draw diagonals to divide the figure into trapeziums and triangles; find the area of each separately, and the sum of the whole equals area.

To find the area of a long irregular figure, bounded on one side by a straight line, (Figs. 9 and 10 on borrowing pits.)

RULE 10.

Multiply one-half the sum of each succeeding height by their distance apart, the product will be the area between the two heights, the sum of all the areas will equal the area of the figure.

To find the area of a circle when the diameter and circumference are both known.

RULE 11.

Multiply the square of the diameter by $\cdot 7854$, or the square of the circumference by $\cdot 07958$; or multiply the circumference by the diameter, and divide the product by 4, will equal area; or one-half the circumference by one-half the diameter.

To find the area of a sector of a circle.

RULE 12.

Multiply the length of the arch by the radius of the circle, and half the product will equal the area, (nearly.)

To find the area of a segment of a circle.

RULE 13.

Multiply the versed sine by the decimal $\cdot 626$; to the square of the product add the square of half the chord; multiply twice the square root of the sum by two-thirds of the versed sine, will equal area.

To find the area of an ellipsis.

RULE 14.

Multiply the transverse or longer diameter by the conjugate or shorter diameter, and by $\cdot 7854$,* will equal area.

To find the area of a circular ring or space included between two concentric circles.

RULE 15.

Add the inside and outside diameters together, multiply the sum by their differences, and by $\cdot 7854$, will equal area.

To find the area of a parabola or its segment.

RULE 16.

Multiply the base by the perpendicular height, and two-thirds of the product equals area.

MENSURATION OF SOLIDS.

To find the solid contents of a cylinder.

RULE 1.

Multiply the area of the base by the height of the cylinder, and the product is the solid contents.

To find the solid contents of a cone or pyramid.

* The area of a circle whose diameter is 1 = $0\cdot 7854$.

RULE 2.

Multiply the area of the base by the perpendicular height, and one-third of the product will equal the solid contents.

To find the solid contents of a frustum of a cone.

RULE 3.

To the product of the diameters of the two ends add the sum of their squares; multiply this sum by the perpendicular height, and by $\cdot 2618$;* the product equals contents.

To find the solid contents of a frustum of a pyramid.

RULE 4.

To the sum of the areas of the two ends add the square root of their product; multiply this sum by the perpendicular height, and one-third of the product equals the contents.

To find the solidity of a wedge.

RULE 5.

To the length of the wedge add twice the length of the base; multiply that sum by the height, and by the breadth of the base, and one-sixth of the product equals contents.

To find the solid contents of a prism.

RULE 6.

Multiply the area of the base by the length, equals contents.

* The solidity of a cone 1 foot diameter and 1 foot high equals $\cdot 2618$.

To find the solid contents of a sphere or globe.

RULE 7.

Multiply the cube of the diameter by $\cdot 5236$; the product equals contents.

To find the solid contents of the segment of a sphere.

RULE 8.

Add the square root of the height to three times the square of the radius of the base; multiply that sum by the height, and by $\cdot 5236$; the product is the contents.

To find the solidity of a spheroid.

RULE 9.

Multiply the square of the least diameter by the length of the greatest diameter, or a line drawn perpendicular to the least diameter, and by $\cdot 5236$; the product will be the solidity.

To find the solidity of a segment of a spheroid, when the base is circular or parallel to the revolving axis or least diameter.

RULE 10.

From triple the fixed axis take double the height of the segment; multiply the difference by the square of the height, and by $\cdot 5236$. Then say, as the square of the fixed axis is to the square of the revolving axis, so is the former product to the solidity.

To find the solid contents of a cylindric ring.

RULE 11.

To the thickness of the ring add the inner diameter; multiply that sum by the square of the thickness, and by 2.4674; the product will be the solid contents.

To find the superficial contents of a board or plank.

RULE 12.

Multiply the length by the width.

If the plank or board are of an unequal breadth at the ends.

RULE 13.

Multiply the average width of the ends by the length.

To find the solidity of timber.

RULE 14.

Multiply the length in feet by the square of one-fourth the girth in inches, gives the solidity in cubic feet.

NOTE.—The above rules No. 12 and 13 only apply when all the dimensions are in feet. When either the length or breadth are given in inches, divide by 12, when all the dimensions are given in inches, divide by 144.

Application to the table of flat or board measure.

Multiply the length by the number in the table corresponding to any given width.

EXAMPLE.—Given a board $16\frac{1}{2}$ feet in length and $9\frac{3}{4}$ inches in breadth.

The number in the table opposite $9\frac{3}{4}$ inches = $.8125 \times 16\frac{1}{2} = 13.4$ square feet.

TABLE TO FACILITATE THE MENSURATION OF
TIMBER, FLAT OR BROAD MEASURE.

Breadth in inches.	Area of a Lineal foot.	Breadth in inches.	Area of a Lineal foot.	Breadth in inches.	Area of a Lineal foot.
$\frac{1}{4}$	·0208	$4\frac{1}{2}$	·3750	$8\frac{3}{4}$	·7292
$\frac{1}{2}$	·0417	$4\frac{3}{4}$	·3958	9	·7500
$\frac{3}{4}$	·0625	5	·4167	$9\frac{1}{4}$	·7708
1	·0834	$5\frac{1}{4}$	·4375	$9\frac{1}{2}$	·7917
$1\frac{1}{4}$	·1042	$5\frac{1}{2}$	·4583	$9\frac{3}{4}$	·8125
$1\frac{1}{2}$	·1250	$4\frac{3}{4}$	·4792	10	·8334
$1\frac{3}{4}$	·1459	6	·5000	$10\frac{1}{4}$	·8542
2	·1667	$6\frac{1}{4}$	·5208	$10\frac{1}{2}$	·8750
$2\frac{1}{4}$	·1875	$6\frac{1}{2}$	·5416	$10\frac{3}{4}$	·8959
$2\frac{1}{2}$	·2084	$6\frac{3}{4}$	·5625	11	·9167
$2\frac{3}{4}$	·2292	7	·5833	$11\frac{1}{4}$	·9375
3	·2500	$7\frac{1}{4}$	·6042	$11\frac{1}{2}$	·9583
$3\frac{1}{4}$	·2708	$7\frac{1}{2}$	·6250	$11\frac{3}{4}$	·9792
$3\frac{1}{2}$	·2916	$7\frac{3}{4}$	·6458		
$3\frac{3}{4}$	·3125	8	·6667		
4	·3334	$8\frac{1}{4}$	·6875		
$4\frac{1}{4}$	·3542	$8\frac{1}{2}$	·7084		

Application of the table of the solidity of timber.

Multiply the area corresponding to the quarter girth in inches by the length in feet.

EXAMPLE.—Given a piece of timber 20 feet long and 12 inches square.

The number opposite 12 inches = $1\cdot000 \times 20 = 20$ cubic feet.

TABLE TO FACILITATE THE MENSURATION OF
THE SOLIDITY OF TIMBER.

1 qr. girth in inches.	Area in feet.	1 qr. girth in inches.	Area in feet.	1 qr. girth in inches.	Area in feet.
6	·250	12 $\frac{1}{4}$	1·042	19	2·506
6 $\frac{1}{4}$	·272	12 $\frac{1}{2}$	1·085	19 $\frac{1}{2}$	2·640
6 $\frac{1}{2}$	·294	12 $\frac{3}{4}$	1·129	20	2·777
6 $\frac{3}{4}$	·317	13	1·174	20 $\frac{1}{2}$	2·917
7	·340	13 $\frac{1}{4}$	1·219	21	3·062
7 $\frac{1}{4}$	·364	13 $\frac{1}{2}$	1·265	21 $\frac{1}{2}$	3·209
7 $\frac{1}{2}$	·390	13 $\frac{3}{4}$	1·313	22	3·362
7 $\frac{3}{4}$	·417	14	1·361	22 $\frac{1}{2}$	3·516
8	·444	14 $\frac{1}{4}$	1·410	23	3·673
8 $\frac{1}{4}$	·472	14 $\frac{1}{2}$	1·460	23 $\frac{1}{2}$	3·835
8 $\frac{1}{2}$	·501	14 $\frac{3}{4}$	1·511	24	4·000
8 $\frac{3}{4}$	·531	15	1·562	24 $\frac{1}{2}$	4·168
9	·562	15 $\frac{1}{4}$	1·615	25	4·340
9 $\frac{1}{4}$	·594	15 $\frac{1}{2}$	1·668	25 $\frac{1}{2}$	4·516
9 $\frac{1}{2}$	·626	15 $\frac{3}{4}$	1·722	26	4·694
9 $\frac{3}{4}$	·659	16	1·777	26 $\frac{1}{2}$	4·876
10	·694	16 $\frac{1}{4}$	1·833	27	5·062
10 $\frac{1}{4}$	·730	16 $\frac{1}{2}$	1·890	27 $\frac{1}{2}$	5·252
10 $\frac{1}{2}$	·766	16 $\frac{3}{4}$	1·948	28	5·444
10 $\frac{3}{4}$	·803	17	2·006	28 $\frac{1}{2}$	5·640
11	·840	17 $\frac{1}{4}$	2·066	29	5·840
11 $\frac{1}{4}$	·878	17 $\frac{1}{2}$	2·126	29 $\frac{1}{2}$	6·044
11 $\frac{1}{2}$	·918	17 $\frac{3}{4}$	2·187	30	6·250
11 $\frac{3}{4}$	·959	18	2·250		
12	1·000	18 $\frac{1}{2}$	2·376		

Scantling is measured the same as timber, by multiplying the end area by the length.

MISCELLANIES.

The dimensions of the United States standard bushel are $18\frac{1}{2}$ inches inside diameter, and 8 in. deep.

A box 24 inches by 16 inches square, and 28 inches deep, will contain a barrel, 5 bushels.

A box 14 inches by 17 inches square, and 14 inches deep, will contain a half barrel.

A box 26 inches by 15·2 inches square, and 8 inches deep, will contain 1 bushel.

A box 12 inches by 11·2 inches square, and 8 inches deep, will contain one-half bushel.

A box 8 inches by 8·4 inches square, and 8 inches deep, will contain 1 peck.

A box 8 inches by 8 inches square, and 4·2 inches deep, will contain 1 gallon.

A box 7 inches by 8 inches square, and 4·8 inches deep, will contain one-half gallon.

A box 4 inches by 4 inches square, and 4·1 inches deep, will contain 1 quart.

To get the number of bushels in any square crib.

RULE 1.

Find the number of cubic feet in the same, and multiply it by 8 and divide it by 10.

Any area in feet multiplied by 6·232, the product is the number of imperial gallons at one foot in depth; or any area in inches multiplied by 0·4328 = gallons.

Any area multiplied by $\cdot 03704$ = the number of cubic yards at one foot in depth.

To determine the amount of imperial gallons in a vessel, the shape of an inverted cone.

RULE 2.

The square of the sum of the diameter at the top and bottom, of which subtract the quotient of the top and bottom; multiply the remainder by $\cdot 7854$, and by one-third the depth = cubic feet; and by $6\cdot 232$ = imperial gallons.

NOTE.— This rule applies where the dimensions are all given in feet.

2d. To the product of the inner diameters add the squares of the inner diameters; multiply the remainder by the depth, and by $\cdot 2618$; divide that by $277\cdot 274$ = gallons, (nearly.)

NOTE.— This rule applies where the dimensions are given in inches.

To determine the contents of imperial gallons in a kettle forming the segment of a circle.

RULE 3.

Three times the square of half the diameter in inches at the mouth, added to the square of the depth, and multiplied by the depth, and by $\cdot 5236$; divide their product by $277\cdot 274$, equals imperial gallons.

The area of a circle in inches, multiplied by the length or thickness in inches, and by $\cdot 263$, equals the weight of cast iron in pounds.

The old English ale gallon contains 282 cubic inches, and the United States gallon contains 231.

English Dry Measure.

8·665	cubic inches	=	1 gill.
34·659	“ “	=	1 pint.
69·318	“ “	=	1 quart.
277·274	“ “	=	1 gallon.
554·548	“ “	=	1 peck.
1·2837	“ feet	=	1 bushel.

English Imperial Wine Measure.

1·604	cubic feet	=	1 anker.
2·888	“ “	=	1 runlet.
6·739	“ “	=	1 tierce.
10·109	“ “	=	1 hogshead.
3·478	“ “	=	1 puncheon.
20·218	“ “	=	1 pipe.
40·435	“ “	=	1 tun.

Dimensions of Drawing Paper.

Wove Antiquarian,	4 feet	4 inches	by	2 feet	7 inches.
Double Elephant,	3	4	“	2	“ 2 “
Atlas,	2	9	“	2	“ 2 “
Columbier,	2	9 $\frac{3}{4}$	“	1	“ 11 “
Elephant,	2	3 $\frac{3}{4}$	“	1	“ 10 $\frac{1}{4}$ “
Imperial,	2	5	“	1	“ 9 $\frac{1}{4}$ “
Super Royal,	2	3	“	1	“ 7 “
Royal,	2	0	“	1	“ 7 “
Medium,	1	10	“	1	“ 6 “
Demy,	1	7 $\frac{1}{2}$	“	1	“ 3 $\frac{1}{2}$ “

*Manner of Calculating the Natural Sines and
Cosines in the Table.*

The radius of a circle being 1, it is known the semi-circumference will equal $3\cdot1415926535898$, &c. Therefore if we divide it by the number of minutes in a semi-circumference (10800) it will equal the sine of 1 minute = $\cdot0002909$ the first seven places in the table.

The natural cosine equals $\sqrt{1 - \text{sine}'^2} = \cdot999999\cdot9577$.

The natural sine and cosine given, the statement would be as follows:

$$\begin{array}{l} 2 \text{ cosine } 1' \times \text{sine } 1' - 0' = \text{sine } 2' \text{ minute.} \\ 2 \quad " \quad 1' \times " \quad 2' - 1' = " \quad 3' \quad " \\ 2 \quad " \quad 1' \times " \quad 3' - 2' = " \quad 4' \quad " \\ 2 \quad " \quad 1' \times " \quad 4' - 3' = " \quad 5' \quad " \end{array}$$

This process can be run to any extent.

With the sine of one minute, and cosine of one minute given, statement second would be as follows:

$$\begin{array}{l} 1' : \text{sine } 2' - \text{sine } 1' :: \text{sine } 2' + \text{sine } 1' : \text{sine } 3' \\ 2' : " \quad 3' - " \quad 1' :: " \quad 3' + " \quad 1' : " \quad 4' \\ 3' : " \quad 4' - " \quad 1' :: " \quad 4' + " \quad 1' : " \quad 5' \\ 4' : " \quad 5' - " \quad 1' :: " \quad 5' + " \quad 1' : " \quad 6' \end{array}$$

The same statement can be applied for degrees:
Thus:

$$\text{sine } 1^\circ : \text{sine } 2^\circ - \text{sine } 1^\circ :: \text{sine } 2^\circ + \text{sine } 1^\circ : \text{sine } 3^\circ, \\ \&c., \&c.$$

The natural sine of any number of degrees of deflexion with chords of 100 ft. may be found by dividing the chord by the radius corresponding to the angle of deflexion in the table of radii.

EXAMPLE.—Given the deflexion angle 3° , radius corresponding in the table of radii would equal 1910 feet and chord 100 feet.

STATEMENT.— $100 \div 1910 = 0.052356$, natural sine of 3° .

NATURAL SINES AND TANGENTS

TO A RADIUS 1.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

0 Deg.

6 Deg.

/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/
0	0.000000	0.00000	Infinite	1.000000	60	0.984808	1.67439	0.59881	0.98481	29
1	0.000299	0.00291	3437.746	0.999701	59	0.984983	1.67500	0.59852	0.98498	28
2	0.000593	0.00582	1718.873	0.999408	58	0.985158	1.67561	0.59823	0.98516	27
3	0.000887	0.00872	1145.915	0.999116	57	0.985333	1.67622	0.59794	0.98534	26
4	0.001186	0.01163	859.4363	0.998824	56	0.985508	1.67683	0.59765	0.98551	25
5	0.001484	0.01454	687.5488	0.998532	55	0.985683	1.67744	0.59736	0.98569	24
6	0.001745	0.01745	572.9572	0.998240	54	0.985858	1.67805	0.59707	0.98587	23
7	0.002003	0.02036	491.1060	0.997948	53	0.986033	1.67866	0.59678	0.98605	22
8	0.002261	0.02267	429.7175	0.997656	52	0.986208	1.67927	0.59649	0.98623	21
9	0.002519	0.02518	381.9709	0.997364	51	0.986383	1.67988	0.59620	0.98640	20
10	0.002780	0.02780	343.7737	0.997072	50	0.986558	1.68049	0.59591	0.98658	19
11	0.003040	0.03040	312.5213	0.996780	49	0.986733	1.68110	0.59562	0.98675	18
12	0.003300	0.03300	286.4777	0.996488	48	0.986908	1.68171	0.59533	0.98693	17
13	0.003560	0.03560	264.4408	0.996196	47	0.987083	1.68232	0.59504	0.98711	16
14	0.003819	0.03819	245.5519	0.995904	46	0.987258	1.68293	0.59475	0.98729	15
15	0.004079	0.04072	229.1816	0.995612	45	0.987433	1.68354	0.59446	0.98746	14
16	0.004338	0.04338	214.8576	0.995320	44	0.987608	1.68415	0.59417	0.98764	13
17	0.004597	0.04594	202.2187	0.995028	43	0.987783	1.68476	0.59388	0.98781	12
18	0.004856	0.04854	190.4641	0.994736	42	0.987958	1.68537	0.59359	0.98798	11
19	0.005115	0.05126	180.0222	0.994444	41	0.988133	1.68598	0.59330	0.98815	10
20	0.005374	0.05377	171.8854	0.994152	40	0.988308	1.68659	0.59301	0.98833	9
21	0.005633	0.05639	165.7001	0.993860	39	0.988483	1.68720	0.59272	0.98851	8
22	0.005892	0.05899	159.4590	0.993572	38	0.988658	1.68781	0.59243	0.98869	7
23	0.006151	0.06160	149.4590	0.993280	37	0.988833	1.68842	0.59214	0.98887	6
24	0.006410	0.06418	143.2571	0.992988	36	0.989008	1.68903	0.59185	0.98905	5
25	0.006669	0.06669	137.5075	0.992696	35	0.989183	1.68964	0.59156	0.98921	4
26	0.006928	0.06928	132.5185	0.992404	34	0.989358	1.69025	0.59127	0.98938	3
27	0.007187	0.07187	127.3213	0.992112	33	0.989533	1.69086	0.59098	0.98956	2
28	0.007446	0.07446	122.7739	0.991820	32	0.989708	1.69147	0.59069	0.98973	1
29	0.007705	0.07705	118.5401	0.991528	31	0.989883	1.69208	0.59040	0.98986	0
30	0.007964	0.07964	114.5886	0.991236	30					

Deg. 89.

Deg. 89.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

1 Deg.

1 Deg.

/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/
0	-0174524	-01745	57-28096	-9998477	60	31	-0284677	-026477	-9996497	29
1	-0177432	-017746	56-35059	-9998426	59	32	-0287585	-026768	-9996419	28
2	-0180341	-018037	55-44151	-9998374	58	33	-0290493	-027059	-9996341	27
3	-0183249	-018328	54-56130	-9998321	57	34	-0293401	-027350	-9996263	26
4	-0186158	-018619	53-71858	-9998267	56	35	-0296309	-027641	-9996185	25
5	-0189066	-018910	52-89211	-9998213	55	36	-0299216	-027932	-9996107	24
6	-0191974	-019201	52-08867	-9998157	54	37	-0302124	-028223	-9996030	23
7	-0194883	-019492	51-30315	-9998101	53	38	-0305032	-028514	-9995952	22
8	-0197791	-019783	50-54880	-9998044	52	39	-0307940	-028805	-9995874	21
9	-0200699	-020074	49-81572	-9997986	51	40	-0310847	-029097	-9995797	20
10	-0203608	-020365	49-10388	-9997927	50	41	-0313755	-029388	-9995720	19
11	-0206516	-020656	48-41208	-9997867	49	42	-0316662	-029679	-9995643	18
12	-0209424	-020947	47-73990	-9997807	48	43	-0319570	-029970	-9995565	17
13	-0212332	-021238	47-08334	-9997745	47	44	-0322478	-030261	-9995488	16
14	-0215241	-021529	46-44886	-9997683	46	45	-0325385	-030552	-9995410	15
15	-0218149	-021820	45-82935	-9997620	45	46	-0328293	-030843	-9995333	14
16	-0221057	-022111	45-22614	-9997556	44	47	-0331200	-031135	-9995257	13
17	-0223965	-022402	44-63859	-9997492	43	48	-0334108	-031426	-9995180	12
18	-0226873	-022693	44-06611	-9997426	42	49	-0337015	-031717	-9995103	11
19	-0229781	-022984	43-50812	-9997360	41	50	-0339922	-032008	-9995026	10
20	-0232689	-023275	42-96407	-9997292	40	51	-0342830	-032299	-9994949	9
21	-0235598	-023566	42-43346	-9997224	39	52	-0345737	-032591	-9994872	8
22	-0238506	-023857	41-91579	-9997156	38	53	-0348644	-032882	-9994795	7
23	-0241414	-024148	41-41058	-9997086	37	54	-0351552	-033173	-9994718	6
24	-0244322	-024439	40-91741	-9997015	36	55	-0354460	-033464	-9994641	5
25	-0247230	-024730	40-43583	-9996943	35	56	-0357368	-033755	-9994564	4
26	-0250138	-025021	39-96546	-9996871	34	57	-0360274	-034047	-9994487	3
27	-0253046	-025312	39-50589	-9996798	33	58	-0363181	-034338	-9994410	2
28	-0255954	-025603	39-05677	-9996724	32	59	-0366088	-034629	-9994333	1
29	-0258862	-025894	38-61773	-9996649	31	60	-0368995	-034920	-9994256	0
30	-0261769	-026185	38-18845	-9996573	30					

Deg. 88.

Deg. 88.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

2 DEG.

2 DEG.

/	/	SINE.	TANG.	COTANG.	COSINE.	/	/	SINE.	TANG.	COTANG.	COSINE.	/	/
0	0	0.000000	0.000000	1.000000	1.000000	60	31	0.9993908	0.43302	2.275189	0.999355	29	
1	1	0.000000	0.000000	1.000000	0.9993908	59	32	0.9993806	0.44243	2.250201	0.999327	28	
2	2	0.000000	0.000000	1.000000	0.9993704	58	33	0.9993604	0.45184	2.225213	0.999300	27	
3	3	0.000000	0.000000	1.000000	0.9993502	57	34	0.9993402	0.46125	2.200225	0.999273	26	
4	4	0.000000	0.000000	1.000000	0.9993300	56	35	0.9993200	0.47066	2.175237	0.999246	25	
5	5	0.000000	0.000000	1.000000	0.9993198	55	36	0.9993100	0.48007	2.150249	0.999219	24	
6	6	0.000000	0.000000	1.000000	0.9993096	54	37	0.9993000	0.48948	2.125261	0.999192	23	
7	7	0.000000	0.000000	1.000000	0.9992994	53	38	0.9992900	0.49889	2.100273	0.999165	22	
8	8	0.000000	0.000000	1.000000	0.9992892	52	39	0.9992800	0.50830	2.075285	0.999138	21	
9	9	0.000000	0.000000	1.000000	0.9992790	51	40	0.9992700	0.51771	2.050297	0.999111	20	
10	10	0.000000	0.000000	1.000000	0.9992688	50	41	0.9992600	0.52712	2.025309	0.999084	19	
11	11	0.000000	0.000000	1.000000	0.9992586	49	42	0.9992500	0.53653	2.000321	0.999057	18	
12	12	0.000000	0.000000	1.000000	0.9992484	48	43	0.9992400	0.54594	1.975333	0.999030	17	
13	13	0.000000	0.000000	1.000000	0.9992382	47	44	0.9992300	0.55535	1.950345	0.999003	16	
14	14	0.000000	0.000000	1.000000	0.9992280	46	45	0.9992200	0.56476	1.925357	0.998976	15	
15	15	0.000000	0.000000	1.000000	0.9992178	45	46	0.9992100	0.57417	1.900369	0.998949	14	
16	16	0.000000	0.000000	1.000000	0.9992076	44	47	0.9992000	0.58358	1.875381	0.998922	13	
17	17	0.000000	0.000000	1.000000	0.9991974	43	48	0.9991900	0.59299	1.850393	0.998895	12	
18	18	0.000000	0.000000	1.000000	0.9991872	42	49	0.9991800	0.60240	1.825405	0.998868	11	
19	19	0.000000	0.000000	1.000000	0.9991770	41	50	0.9991700	0.61181	1.800417	0.998841	10	
20	20	0.000000	0.000000	1.000000	0.9991668	40	51	0.9991600	0.62122	1.775429	0.998814	9	
21	21	0.000000	0.000000	1.000000	0.9991566	39	52	0.9991500	0.63063	1.750441	0.998787	8	
22	22	0.000000	0.000000	1.000000	0.9991464	38	53	0.9991400	0.64004	1.725453	0.998760	7	
23	23	0.000000	0.000000	1.000000	0.9991362	37	54	0.9991300	0.64945	1.700465	0.998733	6	
24	24	0.000000	0.000000	1.000000	0.9991260	36	55	0.9991200	0.65886	1.675477	0.998706	5	
25	25	0.000000	0.000000	1.000000	0.9991158	35	56	0.9991100	0.66827	1.650489	0.998679	4	
26	26	0.000000	0.000000	1.000000	0.9991056	34	57	0.9991000	0.67768	1.625501	0.998652	3	
27	27	0.000000	0.000000	1.000000	0.9990954	33	58	0.9990900	0.68709	1.600513	0.998625	2	
28	28	0.000000	0.000000	1.000000	0.9990852	32	59	0.9990800	0.69650	1.575525	0.998598	1	
29	29	0.000000	0.000000	1.000000	0.9990750	31	60	0.9990700	0.70591	1.550537	0.998571	0	
30	30	0.000000	0.000000	1.000000	0.9990648	30					0.998544		

Deg. 87.

Deg. 87.

NATURAL SINES AND TANGENTS TO A RADIUS 1.
3 DEG.

3 DEG.

/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/
0	0.0000000	0.0000000	19.081113	0.9999999	60	0.6133890	0.64154	1.627217	0.9881770	28
1	0.0174524	0.030909	18.97552	0.998143	61	0.616292	0.64746	1.619322	0.9880041	29
2	0.0349069	0.06191	18.87106	0.995989	62	0.619196	0.65338	1.611839	0.9880811	27
3	0.0523614	0.09292	18.76775	0.993835	63	0.622102	0.65930	1.604348	0.9880581	26
4	0.0698159	0.12393	18.66556	0.991680	64	0.625007	0.66522	1.596856	0.9880350	25
5	0.0872703	0.15494	18.56447	0.989524	65	0.627913	0.67114	1.589364	0.9880120	24
6	0.1047248	0.18595	18.46447	0.987367	66	0.630819	0.67706	1.581872	0.9879889	23
7	0.1221792	0.21696	18.36553	0.985209	67	0.633725	0.68298	1.574380	0.9879658	22
8	0.1396337	0.24797	18.26765	0.983050	68	0.636631	0.68890	1.566888	0.9879427	21
9	0.1570881	0.27898	18.17080	0.980891	69	0.639537	0.69482	1.559396	0.9879196	20
10	0.1745425	0.30999	18.07497	0.978731	70	0.642443	0.70074	1.551904	0.9878965	19
11	0.1919969	0.34100	17.98015	0.976570	71	0.645349	0.70666	1.544412	0.9878734	18
12	0.2094513	0.37201	17.88531	0.974408	72	0.648255	0.71258	1.536920	0.9878503	17
13	0.2269057	0.40302	17.79044	0.972245	73	0.651161	0.71850	1.529428	0.9878272	16
14	0.2443601	0.43403	17.69552	0.970081	74	0.654067	0.72442	1.521936	0.9878041	15
15	0.2618145	0.46504	17.60065	0.967917	75	0.656973	0.73034	1.514444	0.9877810	14
16	0.2792689	0.49605	17.50577	0.965751	76	0.659879	0.73626	1.506952	0.9877579	13
17	0.2967233	0.52706	17.41089	0.963585	77	0.662785	0.74218	1.499460	0.9877348	12
18	0.3141777	0.55807	17.31601	0.961418	78	0.665691	0.74810	1.491968	0.9877117	11
19	0.3316321	0.58908	17.22113	0.959250	79	0.668597	0.75402	1.484476	0.9876886	10
20	0.3490865	0.62009	17.12625	0.957082	80	0.671503	0.76000	1.476984	0.9876655	9
21	0.3665409	0.65110	17.03137	0.954914	81	0.674409	0.76592	1.469492	0.9876424	8
22	0.3839953	0.68211	16.93649	0.952745	82	0.677315	0.77184	1.462000	0.9876193	7
23	0.4014497	0.71312	16.84161	0.950577	83	0.680221	0.77776	1.454508	0.9875962	6
24	0.4189041	0.74413	16.74673	0.948408	84	0.683127	0.78368	1.447016	0.9875731	5
25	0.4363585	0.77514	16.65185	0.946239	85	0.686033	0.78960	1.439524	0.9875500	4
26	0.4538129	0.80615	16.55697	0.944069	86	0.688939	0.79552	1.432032	0.9875269	3
27	0.4712673	0.83716	16.46209	0.941899	87	0.691845	0.80144	1.424540	0.9875038	2
28	0.4887217	0.86817	16.36721	0.939729	88	0.694751	0.80736	1.417048	0.9874807	1
29	0.5061761	0.89918	16.27233	0.937559	89	0.697657	0.81328	1.409556	0.9874576	0
30	0.5236305	0.93019	16.17745	0.935389	90	0.700563	0.81920	1.402064	0.9874345	

Deg. 86.

Deg. 86.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

4 Deg.

4 Deg.

/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/
0	0.697565	0.999926	14.30066	0.9975641	31	0.787491	0.78994	12.65912	0.968945	29
1	0.700467	0.999919	14.24113	0.9975437	32	0.790391	0.79287	12.61239	0.968715	28
2	0.703368	0.999911	14.18209	0.9975233	33	0.793290	0.79579	12.56599	0.968485	27
3	0.706270	0.999903	14.12303	0.9975028	34	0.796189	0.79872	12.51994	0.968254	26
4	0.709171	0.999895	14.06345	0.9974822	35	0.799089	0.80165	12.47432	0.968022	25
5	0.712073	0.999887	14.00385	0.9974615	36	0.801988	0.80458	12.42883	0.967789	24
6	0.714974	0.999878	13.94421	0.9974408	37	0.804887	0.80750	12.38376	0.967555	23
7	0.717876	0.999869	13.88454	0.9974201	38	0.807788	0.81043	12.33902	0.967321	22
8	0.720777	0.999860	13.82486	0.9973994	39	0.810687	0.81336	12.29460	0.967086	21
9	0.723678	0.999851	13.76516	0.9973787	40	0.813587	0.81629	12.25050	0.966851	20
10	0.726579	0.999842	13.70543	0.9973579	41	0.816486	0.81922	12.20671	0.966616	19
11	0.729481	0.999833	13.64568	0.9973372	42	0.819385	0.82215	12.16323	0.966381	18
12	0.732382	0.999824	13.58591	0.9973164	43	0.822284	0.82507	12.12006	0.966145	17
13	0.735283	0.999815	13.52612	0.9972957	44	0.825183	0.82790	12.07719	0.965910	16
14	0.738184	0.999806	13.46633	0.9972749	45	0.828082	0.83083	12.03462	0.965675	15
15	0.741085	0.999797	13.40652	0.9972542	46	0.830981	0.83376	11.99234	0.965440	14
16	0.743986	0.999788	13.34670	0.9972334	47	0.833880	0.83669	11.95037	0.965205	13
17	0.746887	0.999779	13.28687	0.9972126	48	0.836778	0.83962	11.90863	0.964970	12
18	0.749787	0.999770	13.22703	0.9971918	49	0.839677	0.84255	11.86728	0.964735	11
19	0.752688	0.999761	13.16718	0.9971710	50	0.842576	0.84548	11.82616	0.964500	10
20	0.755589	0.999752	13.10732	0.9971502	51	0.845474	0.84839	11.78533	0.964265	9
21	0.758489	0.999743	13.04745	0.9971294	52	0.848373	0.85134	11.74477	0.964030	8
22	0.761390	0.999734	12.98757	0.9971086	53	0.851271	0.85430	11.70440	0.963795	7
23	0.764290	0.999725	12.92768	0.9970878	54	0.854169	0.85723	11.66449	0.963560	6
24	0.767190	0.999716	12.86778	0.9970670	55	0.857067	0.86028	11.62476	0.963325	5
25	0.770091	0.999707	12.80787	0.9970462	56	0.859966	0.86336	11.58529	0.963090	4
26	0.772991	0.999698	12.74795	0.9970254	57	0.862864	0.86649	11.54609	0.962855	3
27	0.775891	0.999689	12.68802	0.9970046	58	0.865762	0.86962	11.50715	0.962620	2
28	0.778791	0.999680	12.62808	0.9969838	59	0.868660	0.87270	11.46847	0.962385	1
29	0.781691	0.999671	12.56813	0.9969630	60	0.871557	0.87588	11.43005	0.962150	0
30	0.784591	0.999662	12.50817	0.9969422	30					

Deg. 85.

Deg. 85.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

5 DEG.

5 DEG.

/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/
0	-.0871557	-.0871558	11.43005	-.9961947	60	31	-.0861353	-.096552	10.83352	28	-.9953683				
1	-.0874445	-.0877831	11.39158	-.9961033	59	32	-.0864248	-.096876	10.82244	29	-.9953403				
2	-.0877353	-.0880774	11.35397	-.9961138	58	33	-.0867144	-.097169	10.8125	27	-.9953122				
3	-.0880251	-.0883698	11.31630	-.9961183	57	34	-.0870039	-.097463	10.80264	26	-.9952840				
4	-.0883148	-.0886661	11.27888	-.9960926	56	35	-.0872934	-.097757	10.79272	25	-.9952557				
5	-.0886046	-.0890554	11.24171	-.9960669	55	36	-.0875829	-.098050	10.78283	24	-.9952274				
6	-.0888943	-.0893447	11.20478	-.9960411	54	37	-.0878724	-.098344	10.77295	23	-.9951990				
7	-.0891840	-.0896354	11.16805	-.9960152	53	38	-.0881619	-.098638	10.76305	22	-.9951705				
8	-.0894738	-.0899284	11.13163	-.9959892	52	39	-.0884508	-.098932	10.75317	21	-.9951419				
9	-.0897635	-.0902127	11.09541	-.9959631	51	40	-.0887408	-.099225	10.74330	20	-.9951132				
10	-.0900532	-.0904920	11.05943	-.9959370	50	41	-.0890303	-.099519	10.73343	19	-.9950844				
11	-.0903429	-.0907713	11.02367	-.9959107	49	42	-.0893197	-.099813	10.72356	18	-.9950556				
12	-.0906326	-.0910507	10.98815	-.9958844	48	43	-.0896092	-.100107	10.71368	17	-.9950268				
13	-.0909223	-.0913300	10.95285	-.9958580	47	44	-.0898986	-.100400	10.70381	16	-.9949979				
14	-.0912119	-.0916093	10.91777	-.9958315	46	45	-.0901881	-.100694	10.69394	15	-.9949689				
15	-.0915016	-.0918887	10.88292	-.9958050	45	46	-.0904775	-.100988	10.68407	14	-.9949398				
16	-.0917913	-.0921680	10.84828	-.9957783	44	47	-.0907669	-.101282	10.67420	13	-.9949107				
17	-.0920809	-.0924473	10.81387	-.9957515	43	48	-.0910563	-.101576	10.66433	12	-.9948816				
18	-.0923706	-.0927367	10.77967	-.9957247	42	49	-.0913457	-.101870	10.65446	11	-.9948521				
19	-.0926602	-.0930060	10.74568	-.9956978	41	50	-.0916351	-.102164	10.64459	10	-.9948227				
20	-.0929499	-.0932854	10.71191	-.9956708	40	51	-.0919245	-.102458	10.63472	9	-.9947932				
21	-.0932395	-.0935647	10.67834	-.9956437	39	52	-.0922139	-.102752	10.62485	8	-.9947637				
22	-.0935291	-.0938440	10.64499	-.9956165	38	53	-.0925032	-.103046	10.61498	7	-.9947342				
23	-.0938187	-.0941234	10.61184	-.9955892	37	54	-.0927925	-.103339	10.60511	6	-.9947047				
24	-.0941083	-.0944031	10.57889	-.9955620	36	55	-.0930819	-.103634	10.59524	5	-.9946752				
25	-.0943979	-.0946921	10.54615	-.9955345	35	56	-.0933712	-.103928	10.58537	4	-.9946457				
26	-.0946875	-.0949811	10.51360	-.9955070	34	57	-.0936605	-.104222	10.57550	3	-.9946162				
27	-.0949771	-.0952701	10.48126	-.9954794	33	58	-.0939499	-.104516	10.56563	2	-.9945865				
28	-.0952666	-.0955601	10.44911	-.9954517	32	59	-.0942392	-.104810	10.55576	1	-.9945572				
29	-.0955562	-.0958509	10.41715	-.9954240	31	60	-.0945285	-.105104	10.54589	0	-.9945279				
30	-.0958458	-.0962509	10.38539	-.9953962	30										

Deg. 84.

Deg. 84.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

6 Deg.

6 Deg.

/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/
0	.1045285	.105104	.9514364	.9945219	60	.1134922	.114230	.8754246	.9935389	29
1	.1048178	.105398	.9487814	.99446914	59	.1137812	.114525	.8731719	.9935068	28
2	.1051070	.105692	.9461411	.9944169	58	.1140702	.114819	.8709307	.9934727	27
3	.1053963	.105986	.9435153	.9943643	57	.1143592	.115114	.8687008	.9934395	26
4	.1056856	.106280	.9408988	.9943116	56	.1146482	.115409	.8664822	.9934062	25
5	.1059748	.106575	.9383066	.9942588	55	.1149372	.115703	.8642747	.9933728	24
6	.1062641	.106869	.9357235	.9942059	54	.1152261	.115998	.8620753	.9933393	23
7	.1065533	.107163	.9331546	.9941530	53	.1155151	.116293	.8598929	.9933057	22
8	.1068425	.107457	.9305803	.9941001	52	.1158040	.116588	.8577183	.9932721	21
9	.1071318	.107751	.9280060	.9940472	51	.1160929	.116883	.8555546	.9932384	20
10	.1074210	.108046	.9254318	.9940448	50	.1163818	.117178	.8534017	.9932045	19
11	.1077102	.108340	.9228575	.9940424	49	.1166707	.117473	.8512504	.9931706	18
12	.1079994	.108634	.9202832	.9941510	48	.1169596	.117767	.8491277	.9931367	17
13	.1082885	.108928	.9177089	.9941980	47	.1172485	.118062	.8470065	.9931028	16
14	.1085777	.109223	.9151346	.9942458	46	.1175374	.118357	.8448857	.9930685	15
15	.1088669	.109517	.9125603	.9942936	45	.1178263	.118652	.8427653	.9930342	14
16	.1091560	.109812	.9100044	.9943414	44	.1181151	.118947	.8406451	.9929999	13
17	.1094452	.110106	.9074485	.9943892	43	.1184040	.119242	.8385251	.9929655	12
18	.1097343	.110401	.9048926	.9944370	42	.1186928	.119537	.8364053	.9929310	11
19	.1100234	.110695	.9023367	.9944848	41	.1189816	.120127	.8342857	.9928965	10
20	.1103126	.110989	.9000000	.9945326	40	.1192704	.120423	.8321661	.9928621	9
21	.1106017	.111284	.8978834	.9945804	39	.1195593	.120718	.8300465	.9928277	8
22	.1108908	.111578	.8959667	.9946282	38	.1198481	.121013	.8279271	.9927932	7
23	.1111799	.111873	.8942500	.9946760	37	.1201368	.121308	.8258075	.9927587	6
24	.1114690	.112168	.8927333	.9947238	36	.1204256	.121603	.8236879	.9927242	5
25	.1117580	.112462	.8913166	.9947716	35	.1207144	.121898	.8215683	.9926897	4
26	.1120471	.112757	.8899999	.9948194	34	.1210031	.122193	.8194487	.9926552	3
27	.1123361	.113051	.8887832	.9948672	33	.1212919	.122488	.8173291	.9926207	2
28	.1126252	.113346	.8876665	.9949150	32	.1215806	.122783	.8152095	.9925861	1
29	.1129142	.113641	.8866498	.9949628	31	.1218693		.8130900	.9925516	0
30	.1132032	.113936	.8857331	.9950106	30			.8110000		

Deg. 83

Deg. 83.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

7 DEG.

7 DEG.

/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/
0	.1218603	.122784	8.144346	.9925462	60	.31			.9308146	
1	.1221581	.123078	8.124807	.9925107	59	32	.131080	.132244	.7578717	28
2	.1224468	.123375	8.105359	.9924751	58	33	.1313913	.132540	.7561756	29
3	.1227355	.123670	8.086004	.9924394	57	34	.1317037	.132836	.7544859	26
4	.1230241	.123965	8.066739	.9924037	56	35	.1320161	.133132	.7528057	27
5	.1233128	.124261	8.047564	.9923679	55	36	.1323285	.133428	.7511317	25
6	.1236015	.124556	8.028479	.9923319	54	37	.1326407	.133724	.7494651	24
7	.1238901	.124852	8.009483	.9922959	53	38	.1329530	.134020	.7478057	23
8	.1241788	.125147	7.990575	.9922599	52	39	.1332653	.134316	.7461535	22
9	.1244674	.125442	7.971756	.9922237	51	40	.1335776	.134612	.7445085	21
10	.1247560	.125738	7.953022	.9921874	50	41	.1338899	.134909	.7428706	20
11	.1250446	.126033	7.934375	.9921511	49	42	.1342022	.135205	.7412387	19
12	.1253332	.126329	7.915815	.9921147	48	43	.1345144	.135501	.7396159	18
13	.1256218	.126624	7.897339	.9920782	47	44	.1348267	.135797	.7379990	17
14	.1259104	.126920	7.878948	.9920416	46	45	.1351389	.136094	.7363881	16
15	.1261990	.127216	7.860642	.9920049	45	46	.1354512	.136390	.7347851	15
16	.1264875	.127511	7.842419	.9919682	44	47	.1357635	.136686	.7331898	14
17	.1267761	.127807	7.824271	.9919314	43	48	.1360758	.136983	.7316004	13
18	.1270646	.128103	7.806229	.9918944	42	49	.1363881	.137279	.7300178	12
19	.1273531	.128398	7.788245	.9918574	41	50	.1367004	.137575	.7284418	11
20	.1276416	.128694	7.770350	.9918204	40	51	.1370127	.137872	.7268725	10
21	.1279302	.128990	7.752536	.9917832	39	52	.1373250	.138168	.7253098	9
22	.1282188	.129285	7.734802	.9917469	38	53	.1376373	.138465	.7237537	8
23	.1285071	.129581	7.717148	.9917106	37	54	.1379496	.138761	.7222042	7
24	.1287956	.129877	7.699573	.9916742	36	55	.1382619	.139058	.7206611	6
25	.1290841	.130173	7.682076	.9916377	35	56	.1385742	.139354	.7191245	5
26	.1293725	.130469	7.664658	.9916011	34	57	.1388865	.139651	.7175943	4
27	.1296609	.130764	7.647317	.9915644	33	58	.1391988	.139947	.7160705	3
28	.1299494	.131060	7.630063	.9915276	32	59	.1395111	.140244	.7145530	2
29	.1302378	.131356	7.612885	.9914908	31	60	.1398234	.140540	.7130419	1
30	.1305262	.131652	7.595754	.9914549	30				.7115369	0

Deg. 82.

Deg. 82.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

8 DEG.

8 DEG.

/	/	SINE.	TANG.	COTANG.	COSINE.	/	/	SINE.	TANG.	COTANG.	COSINE.	/
0	1	-.1391731	-.140540	7.115369	-.9902681	59	31	-.1480971	-.149748	6.677867	-.9899728	29
1	2	-.1397412	-.141037	7.100852	-.9902275	60	32	-.1486348	-.150045	6.664680	-.9899297	28
2	3	-.1397492	-.141130	7.085457	-.9901869	58	33	-.1486724	-.150343	6.651444	-.9898805	27
3	4	-.1403772	-.141330	7.070593	-.9901462	57	34	-.1489601	-.150640	6.638310	-.9898312	26
4	5	-.1408262	-.141727	7.055790	-.9901055	56	35	-.1492477	-.150938	6.625225	-.9897908	25
5	6	-.1401332	-.142024	7.041048	-.9900646	55	36	-.1495353	-.151235	6.612191	-.9897504	24
6	7	-.1409012	-.142321	7.026266	-.9900237	54	37	-.1498230	-.151533	6.599278	-.9897128	23
7	8	-.1417892	-.142617	7.011744	-.9899826	53	38	-.1501106	-.151830	6.586273	-.9896662	22
8	9	-.1417651	-.142914	6.997180	-.9899415	52	39	-.1503981	-.152128	6.573389	-.9896255	21
9	10	-.1420531	-.143211	6.982678	-.9899003	51	40	-.1506857	-.152426	6.560553	-.9895817	20
10	11	-.1423410	-.143508	6.968283	-.9898590	50	41	-.1509733	-.152723	6.547767	-.9895378	19
11	12	-.1426289	-.143805	6.953847	-.9898177	49	42	-.1512608	-.153021	6.535029	-.9894939	18
12	13	-.1429168	-.144102	6.939319	-.9897762	48	43	-.1515484	-.153319	6.522339	-.9894498	17
13	14	-.1432047	-.144399	6.924748	-.9897347	47	44	-.1518359	-.153617	6.509696	-.9894057	16
14	15	-.1434926	-.144696	6.910185	-.9896931	46	45	-.1521234	-.153914	6.497104	-.9893615	15
15	16	-.1437805	-.144993	6.895679	-.9896514	45	46	-.1524109	-.154212	6.484558	-.9893172	14
16	17	-.1437805	-.145290	6.882780	-.9896096	44	47	-.1526984	-.154510	6.472059	-.9892728	13
17	18	-.1440684	-.145587	6.869737	-.9895677	43	48	-.1529858	-.154808	6.459607	-.9892284	12
18	19	-.1443562	-.145884	6.856750	-.9895258	42	49	-.1532733	-.155106	6.447201	-.9891838	11
19	20	-.1446440	-.146181	6.843819	-.9894838	41	50	-.1535607	-.155404	6.434842	-.9891392	10
20	21	-.1449319	-.146478	6.830943	-.9894416	40	51	-.1538482	-.155701	6.422530	-.9890945	9
21	22	-.1452197	-.146775	6.818122	-.9893994	39	52	-.1541356	-.156000	6.410283	-.9890497	8
22	23	-.1455075	-.147072	6.805356	-.9893572	38	53	-.1544230	-.156297	6.398042	-.9890048	7
23	24	-.1457953	-.147369	6.792644	-.9893148	37	54	-.1547104	-.156595	6.385866	-.9889599	6
24	25	-.1460830	-.147667	6.779986	-.9892723	36	55	-.1549978	-.156893	6.373735	-.9889148	5
25	26	-.1463708	-.147964	6.767382	-.9892302	35	56	-.1552851	-.157191	6.361650	-.9888697	4
26	27	-.1466585	-.148261	6.754831	-.9891872	34	57	-.1555725	-.157490	6.349609	-.9888245	3
27	28	-.1469463	-.148559	6.742334	-.9891445	33	58	-.1558598	-.157788	6.337612	-.9887792	2
28	29	-.1472340	-.148856	6.729889	-.9891017	32	59	-.1561472	-.158086	6.325660	-.9887338	1
29	30	-.1475217	-.149153	6.717496	-.9890588	31	60	-.1564345	-.158384	6.313751	-.9886883	0
30		-.1478094	-.149451	6.691156	-.9890159	30						

DEG. 81.

DEG. 81.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

9 Deg.

9 Deg.

/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/
0	1.564345	1.58384	6.313751	.9876883	60	1.653345	1.67641	5.963104	.9862375	29
1	1.567218	1.58682	6.301886	.9876428	59	1.656214	1.67940	5.954481	.9861894	28
2	1.570091	1.58980	6.290065	.9875972	58	1.659082	1.68239	5.945895	.9861412	27
3	1.572963	1.59279	6.278286	.9875514	57	1.661951	1.68539	5.937345	.9860929	26
4	1.575836	1.59577	6.266551	.9875057	56	1.664819	1.68838	5.928832	.9860445	25
5	1.578708	1.59875	6.254858	.9874598	55	1.667687	1.69137	5.920355	.9859960	24
6	1.581581	1.60174	6.243208	.9874138	54	1.670556	1.69436	5.911913	.9859475	23
7	1.584453	1.60472	6.231600	.9873678	53	1.673423	1.69735	5.903508	.9858988	22
8	1.587325	1.60770	6.220034	.9873216	52	1.676291	1.70035	5.895138	.9858501	21
9	1.590197	1.61069	6.208510	.9872754	51	1.679159	1.70334	5.886804	.9858013	20
10	1.593069	1.61367	6.197027	.9872291	50	1.682026	1.70633	5.878505	.9857524	19
11	1.595940	1.61664	6.185586	.9871827	49	1.684894	1.70933	5.870241	.9857035	18
12	1.598812	1.61964	6.174186	.9871363	48	1.687761	1.71232	5.862011	.9856544	17
13	1.601683	1.62263	6.162827	.9870897	47	1.690628	1.71532	5.853817	.9856053	16
14	1.604555	1.62561	6.151508	.9870431	46	1.693496	1.71831	5.845631	.9855561	15
15	1.607426	1.62860	6.140230	.9869964	45	1.696362	1.72130	5.837501	.9855068	14
16	1.610297	1.63159	6.128992	.9869496	44	1.699228	1.72430	5.829440	.9854574	13
17	1.613167	1.63457	6.117794	.9869027	43	1.702095	1.72730	5.821352	.9854079	12
18	1.616038	1.63756	6.106636	.9868557	42	1.704961	1.73029	5.813308	.9853583	11
19	1.618909	1.64053	6.095517	.9868087	41	1.707828	1.73329	5.805308	.9853087	10
20	1.621779	1.64353	6.084438	.9867615	40	1.710694	1.73628	5.797342	.9852592	9
21	1.624650	1.64652	6.073397	.9867143	39	1.713560	1.73928	5.789412	.9852097	8
22	1.627520	1.64951	6.062396	.9866670	38	1.716425	1.74228	5.781508	.9851603	7
23	1.630390	1.65250	6.051434	.9866196	37	1.719291	1.74527	5.773639	.9851108	6
24	1.633260	1.65548	6.040510	.9865722	36	1.722156	1.74827	5.765791	.9850613	5
25	1.636129	1.65847	6.029624	.9865246	35	1.725022	1.75127	5.757912	.9850119	4
26	1.638999	1.66145	6.018777	.9864770	34	1.727887	1.75427	5.750066	.9849629	3
27	1.641868	1.66445	6.007967	.9864293	33	1.730752	1.75727	5.742309	.9849139	2
28	1.644738	1.66743	6.007195	.9863815	32	1.733617	1.76027	5.734544	.9848652	1
29	1.647607	1.67043	6.006461	.9863336	31	1.736482	1.76327	5.726781	.9848178	0
30	1.650476	1.67342	5.975764	.9862856	30					

Deg. 80.

Deg. 80.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

10 DEG.

10 DEG.

/	SINE.	TANG.	COTANG.	COSINE.	/	/	SINE.	TANG.	COTANG.	COSINE.	/
0	.1736482	.176327	.5671281	.9848078	60	31	.1825215	.186639	.5386771	.9832019	29
1	.1736346	.176326	.5671650	.9847572	59	32	.1823075	.186640	.5378063	.9831487	28
2	.1736211	.176325	.5672021	.9847066	58	33	.1820935	.186641	.5369353	.9830955	27
3	.1736075	.176324	.5672392	.9846560	57	34	.1818795	.186642	.5360649	.9830422	26
4	.1735939	.176323	.5672763	.9846054	56	35	.1816654	.186643	.5351945	.9829888	25
5	.1735803	.176322	.5673134	.9845548	55	36	.1814514	.186644	.5343241	.9829353	24
6	.1735667	.176321	.5673505	.9845042	54	37	.1812373	.186645	.5334537	.9828818	23
7	.1735531	.176320	.5673876	.9844536	53	38	.1810232	.186646	.5325833	.9828282	22
8	.1735395	.176319	.5674247	.9844030	52	39	.1808091	.186647	.5317129	.9827744	21
9	.1735258	.176318	.5674618	.9843524	51	40	.1805950	.186648	.5308425	.9827206	20
10	.1735121	.176317	.5674989	.9843018	50	41	.1803809	.186649	.5300001	.9826668	19
11	.1734984	.176316	.5675360	.9842512	49	42	.1801668	.186650	.5291577	.9826128	18
12	.1734847	.176315	.5675731	.9842006	48	43	.1800027	.186651	.5283152	.9825587	17
13	.1734710	.176314	.5676102	.9841500	47	44	.1797886	.186652	.5274727	.9825046	16
14	.1734573	.176313	.5676473	.9841000	46	45	.1795745	.186653	.5266302	.9824504	15
15	.1734436	.176312	.5676844	.9840500	45	46	.1793604	.186654	.5257877	.9823961	14
16	.1734299	.176311	.5677215	.9840000	44	47	.1791463	.186655	.5249452	.9823417	13
17	.1734162	.176310	.5677586	.9839500	43	48	.1789322	.186656	.5241027	.9822873	12
18	.1734025	.176309	.5677957	.9839000	42	49	.1787181	.186657	.5232602	.9822327	11
19	.1733888	.176308	.5678328	.9838500	41	50	.1785040	.186658	.5224177	.9821781	10
20	.1733751	.176307	.5678699	.9838000	40	51	.1782900	.186659	.5215752	.9821234	9
21	.1733614	.176306	.5679070	.9837500	39	52	.1780759	.186660	.5207327	.9820686	8
22	.1733477	.176305	.5679441	.9837000	38	53	.1778618	.186661	.5198902	.9820137	7
23	.1733340	.176304	.5679812	.9836500	37	54	.1776477	.186662	.5190477	.9819587	6
24	.1733203	.176303	.5680183	.9836000	36	55	.1774336	.186663	.5182052	.9819037	5
25	.1733066	.176302	.5680554	.9835500	35	56	.1772195	.186664	.5173627	.9818485	4
26	.1732929	.176301	.5680925	.9835000	34	57	.1770054	.186665	.5165202	.9817930	3
27	.1732792	.176300	.5681296	.9834500	33	58	.1767913	.186666	.5156777	.9817372	2
28	.1732655	.176299	.5681667	.9834000	32	59	.1765772	.186667	.5148352	.9816816	1
29	.1732518	.176298	.5682038	.9833500	31	60	.1763631	.186668	.5139927	.9816257	0

Deg. 79.

Deg. 79.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

11 DEG.

11 DEG.

/	SINE.	TANG.	COTANG.	COSINE.	/	/	SINE.	TANG.	COTANG.	COSINE.	/
0	.190890	.194380	5.144554	.9816272	60	31	.1994530	.203755	4.907849	.9798667	29
1	.1910345	.194582	5.136376	.9815716	59	32	.1996930	.204058	4.900562	.9798086	28
2	.1911801	.194784	5.128222	.9815160	58	33	.1999330	.204361	4.893295	.9797504	27
3	.1913256	.194986	5.120092	.9814603	57	34	.2001730	.204664	4.886049	.9796921	26
4	.1914711	.195188	5.111785	.9814045	56	35	.2004130	.204967	4.878824	.9796337	25
5	.1916166	.195389	5.103490	.9813486	55	36	.2006529	.205270	4.871620	.9795752	24
6	.1917621	.195590	5.095206	.9812927	54	37	.2008929	.205573	4.864435	.9795167	23
7	.1919076	.195792	5.086926	.9812366	53	38	.2011329	.205876	4.857271	.9794581	22
8	.1920531	.195994	5.078646	.9811805	52	39	.2013729	.206180	4.850128	.9793994	21
9	.1921986	.196196	5.070362	.9811243	51	40	.2016129	.206483	4.843004	.9793406	20
10	.1923441	.196398	5.062078	.9810680	50	41	.2018529	.206786	4.835901	.9792818	19
11	.1924896	.196600	5.053794	.9810116	49	42	.2020929	.207090	4.828817	.9792228	18
12	.1926351	.196802	5.045509	.9809552	48	43	.2023329	.207393	4.821753	.9791638	17
13	.1927806	.197004	5.037225	.9808986	47	44	.2025729	.207696	4.814709	.9791047	16
14	.1929261	.197206	5.028940	.9808420	46	45	.2028129	.208000	4.807655	.9790455	15
15	.1930716	.197408	5.020655	.9807853	45	46	.2030529	.208303	4.800600	.9789862	14
16	.1932171	.197610	5.012370	.9807285	44	47	.2032929	.208607	4.793545	.9789268	13
17	.1933626	.197812	5.004085	.9806716	43	48	.2035329	.208910	4.786490	.9788674	12
18	.1935081	.198014	4.995800	.9806147	42	49	.2037729	.209214	4.779435	.9788079	11
19	.1936536	.198216	4.987515	.9805576	41	50	.2040129	.209518	4.772380	.9787483	10
20	.1937991	.198418	4.979230	.9805005	40	51	.2042529	.209821	4.765325	.9786886	9
21	.1939446	.198620	4.970945	.9804433	39	52	.2044929	.210125	4.758270	.9786288	8
22	.1940901	.198822	4.962660	.9803860	38	53	.2047329	.210429	4.751215	.9785689	7
23	.1942356	.199024	4.954375	.9803286	37	54	.2049729	.210733	4.744160	.9785090	6
24	.1943811	.199226	4.946090	.9802712	36	55	.2052129	.211036	4.737105	.9784490	5
25	.1945266	.199428	4.937805	.9802136	35	56	.2054529	.211340	4.730050	.9783889	4
26	.1946721	.199630	4.929520	.9801560	34	57	.2056929	.211644	4.723000	.9783287	3
27	.1948176	.199832	4.921235	.9800983	33	58	.2059329	.211948	4.715945	.9782684	2
28	.1949631	.200034	4.912950	.9800405	32	59	.2061729	.212252	4.708890	.9782080	1
29	.1951086	.200236	4.904665	.9799827	31	60	.2064129	.212556	4.701835	.9781476	0
30	.1952541	.200438	4.896380	.9799247	30						

Deg. 78.

Deg. 78.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

12 DEG.

12 DEG.

/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/
0	.2079117	.212556	.4704530	.9781476	60	.31	.2167256	.221999	.4504507	29
1	.2081962	.212860	.4697310	.9780871	59	32	.2170076	.222305	.4498322	28
2	.2084807	.213164	.4691208	.9780265	58	33	.2172915	.222610	.4492153	27
3	.2087652	.213468	.4685254	.9779658	57	34	.2175754	.222915	.4486000	26
4	.2090497	.213773	.4679350	.9779050	56	35	.2178593	.223221	.4479863	25
5	.2093341	.214077	.4673412	.9778441	55	36	.2181432	.223526	.4473742	24
6	.2096186	.214381	.4667483	.9777832	54	37	.2184271	.223831	.4467637	23
7	.2099030	.214685	.4661572	.9777222	53	38	.2187110	.224137	.4461548	22
8	.2101874	.214990	.4655678	.9776611	52	39	.2189948	.224442	.4455475	21
9	.2104718	.215294	.4649803	.9776000	51	40	.2192786	.224748	.4449418	20
10	.2107561	.215598	.4643924	.9775386	50	41	.2195624	.225054	.4443376	19
11	.2110405	.215903	.4638045	.9774773	49	42	.2198462	.225359	.4437350	18
12	.2113248	.216207	.4632183	.9774159	48	43	.2201300	.225665	.4431339	17
13	.2116091	.216512	.4626328	.9773544	47	44	.2204137	.225971	.4425343	16
14	.2118934	.216816	.4620478	.9772928	46	45	.2206974	.226276	.4419364	15
15	.2121777	.217121	.4614620	.9772311	45	46	.2209811	.226582	.4413399	14
16	.2124619	.217425	.4608768	.9771693	44	47	.2212648	.226888	.4407450	13
17	.2127462	.217730	.4602925	.9771075	43	48	.2215485	.227194	.4401516	12
18	.2130304	.218035	.4597081	.9770456	42	49	.2218321	.227500	.4395597	11
19	.2133146	.218340	.4591242	.9769836	41	50	.2221158	.227806	.4389694	10
20	.2135988	.218644	.4585408	.9769215	40	51	.2223994	.228112	.4383805	9
21	.2138829	.218949	.4579582	.9768593	39	52	.2226830	.228418	.4377931	8
22	.2141671	.219254	.4573761	.9767970	38	53	.2229666	.228724	.4372073	7
23	.2144512	.219559	.4567947	.9767347	37	54	.2232501	.229030	.4366229	6
24	.2147353	.219864	.4562130	.9766723	36	55	.2235337	.229336	.4360400	5
25	.2150194	.220169	.4556317	.9766098	35	56	.2238172	.229642	.4354586	4
26	.2153035	.220474	.4550507	.9765472	34	57	.2241007	.229949	.4348786	3
27	.2155876	.220779	.4544694	.9764845	33	58	.2243842	.230255	.4342901	2
28	.2158716	.221084	.4538881	.9764217	32	59	.2246676	.230561	.4337031	1
29	.2161556	.221389	.4533066	.9763589	31	60	.2249511	.230868	.4331173	0
30	.2164396	.221694	.4527250	.9762960	30					

DEG. 77.

DEG. 77

NATURAL SINES AND TANGENTS TO A RADIUS 1.

13 DEG.

13 DEG.

/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/
0	.2249511	.230868	4.331475	.9743701	31	.2537282	.240386	4.159908	.9723070	29
1	.2252345	.231174	4.325734	.9743046	59	.2440110	.240694	4.154650	.9722339	28
2	.2255179	.231481	4.320007	.9742390	58	.2342938	.241001	4.149344	.9721608	27
3	.2258013	.231787	4.314295	.9741734	57	.2345766	.241309	4.144051	.9720876	26
4	.2260846	.232094	4.308597	.9741077	56	.2348594	.241617	4.138771	.9720144	25
5	.2263680	.232400	4.302913	.9740419	55	.2351421	.241925	4.133504	.9719410	24
6	.2266513	.232707	4.297244	.9739760	54	.2354248	.242233	4.128249	.9718676	23
7	.2269346	.233014	4.291588	.9739100	53	.2357075	.242541	4.123007	.9717942	22
8	.2272179	.233320	4.285947	.9738439	52	.2359902	.242849	4.117778	.9717208	21
9	.2275012	.233627	4.280319	.9737778	51	.2362729	.243157	4.112561	.9716474	20
10	.2277844	.233934	4.274706	.9737116	50	.2365555	.243465	4.107356	.9715740	19
11	.2280677	.234241	4.269107	.9736453	49	.2368381	.243773	4.102164	.9715006	18
12	.2283509	.234547	4.263521	.9735789	48	.2371207	.244081	4.096985	.9714272	17
13	.2286341	.234854	4.257950	.9735124	47	.2374033	.244390	4.091817	.9713538	16
14	.2289172	.235161	4.252392	.9734458	46	.2376859	.244698	4.086652	.9712804	15
15	.2292004	.235468	4.246848	.9733792	45	.2379685	.245006	4.081519	.9712070	14
16	.2294835	.235775	4.241317	.9733125	44	.2382510	.245315	4.076389	.9711336	13
17	.2297666	.236082	4.235800	.9732457	43	.2385335	.245623	4.071270	.9710602	12
18	.2300497	.236390	4.230297	.9731789	42	.2388159	.245932	4.066164	.9709868	11
19	.2303328	.236697	4.224808	.9731119	41	.2390984	.246240	4.061070	.9709134	10
20	.2306159	.237004	4.219331	.9730449	40	.2393808	.246549	4.055987	.9708399	9
21	.2308989	.237311	4.213869	.9729777	39	.2396633	.246857	4.050917	.9707665	8
22	.2311819	.237618	4.208419	.9729105	38	.2399457	.247166	4.045859	.9706931	7
23	.2314649	.237926	4.202983	.9728432	37	.2402280	.247475	4.040812	.9706196	6
24	.2317479	.238233	4.197560	.9727759	36	.2405104	.247783	4.035777	.9705462	5
25	.2320309	.238541	4.192151	.9727084	35	.2407927	.248092	4.030755	.9704728	4
26	.2323138	.238848	4.186754	.9726409	34	.2410751	.248401	4.025744	.9703993	3
27	.2325967	.239156	4.181371	.9725733	33	.2413574	.248710	4.020744	.9703259	2
28	.2328796	.239463	4.176001	.9725056	32	.2416398	.249019	4.015757	.9702524	1
29	.2331625	.239771	4.170644	.9724378	31	.2419219	.249328	4.010780	.9701789	0
30	.2334454	.240078	4.165289	.9723699	30					

Deg. 76.

Deg. 76.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

14 Deg.

14 Deg.

/	/	SINE.	TANG.	COTANG.	COSINE.	/	/	SINE.	TANG.	COTANG.	COSINE.	/
0	1	2419219	243928	4.010780	97.02357	59	31	2506616	258928	3.862078	96800748	29
1	2	2422041	244637	4.005816	97.02253	60	32	2509238	256298	3.857453	96800748	28
2	3	2424863	246946	4.000863	97.01548	58	33	2511063	256548	3.852839	9679288	27
3	4	2427685	250255	3.995922	97.00842	57	34	2512885	256859	3.848255	9678507	26
4	5	2430507	253564	3.990972	97.00135	56	35	2514707	257169	3.843642	9677725	25
5	6	2433329	256873	3.986023	96.99428	55	36	2516529	257480	3.839059	9676943	24
6	7	2436150	260182	3.981166	96.98720	54	37	2518351	257791	3.834486	9676162	23
7	8	2438971	263491	3.976311	96.98011	53	38	2520173	258102	3.829923	9675380	22
8	9	2441792	266800	3.971454	96.97301	52	39	2521995	258412	3.825370	9674598	21
9	10	2444613	270109	3.966597	96.96591	51	40	2523817	258723	3.820828	9673816	20
10	11	2447435	273418	3.961740	96.95879	50	41	2525639	259034	3.816285	9673034	19
11	12	2450257	276727	3.956883	96.95167	49	42	2527461	259345	3.811742	9672252	18
12	13	2453079	280036	3.952026	96.94453	48	43	2529283	259656	3.807200	9671470	17
13	14	2455901	283345	3.947169	96.93740	47	44	2531105	259967	3.802658	9670688	16
14	15	2458723	286654	3.942312	96.93025	46	45	2532927	260278	3.798115	9669906	15
15	16	2461545	289963	3.937455	96.92309	45	46	2534749	260589	3.793573	9669124	14
16	17	2464367	293272	3.932598	96.91593	44	47	2536571	260900	3.789030	9668342	13
17	18	2467189	296581	3.927741	96.90875	43	48	2538393	261211	3.784488	9667560	12
18	19	2469990	299890	3.922884	96.90157	42	49	2540215	261522	3.779945	9666778	11
19	20	2472809	303200	3.918027	96.89438	41	50	2542037	261833	3.775403	9665996	10
20	21	2475627	306509	3.913170	96.88719	40	51	2543859	262144	3.770860	9665214	9
21	22	2478445	309818	3.908313	96.87998	39	52	2545681	262455	3.766317	9664432	8
22	23	2481263	313127	3.903456	96.87277	38	53	2547503	262766	3.761774	9663650	7
23	24	2484081	316436	3.898599	96.86555	37	54	2549325	263077	3.757231	9662868	6
24	25	2486899	319745	3.893742	96.85832	36	55	2551147	263388	3.752688	9662086	5
25	26	2489717	323054	3.888885	96.85108	35	56	2552969	263699	3.748145	9661304	4
26	27	2492535	326363	3.884028	96.84383	34	57	2554791	264010	3.743602	9660522	3
27	28	2495353	329672	3.879171	96.83658	33	58	2556613	264321	3.739059	9659740	2
28	29	2498171	332981	3.874314	96.82933	32	59	2558435	264632	3.734516	9658958	1
29	30	2500989	336290	3.869457	96.82208	31	60	2560257	264943	3.729973	9658176	0
30		2503807	339600	3.864600	96.81483	30		2562079	265254	3.725430	9657394	

DEG. 7.

DEG. 75.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

16 DEG.

16 DEG.

/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/
0	2756374	286745	3487414	9612617	60	31	2842942	296529	9587371	29
1	2759170	287040	3483589	9611815	59	32	2845731	296846	9586543	28
2	2761965	287375	3479772	9611012	58	33	2848520	297163	9585715	27
3	2764761	287700	3475963	9610208	57	34	2851308	297479	9584886	26
4	2767556	288005	3472151	9609403	56	35	2854096	297796	9584056	25
5	2770352	288320	3468367	9608598	55	36	2856884	298112	9583226	24
6	2773147	288635	3464581	9607792	54	37	2859671	298429	9582394	23
7	2775941	288950	3460802	9606984	53	38	2862458	298746	9581562	22
8	2778736	289265	3457031	9606177	52	39	2865246	299063	9580729	21
9	2781530	289580	3453267	9605368	51	40	2868032	299380	9579895	20
10	2784324	289896	3449512	9604558	50	41	2870819	299697	9579060	19
11	2787118	290211	3445763	9603748	49	42	2873605	299968	9578225	18
12	2789911	290526	3442022	9602937	48	43	2876391	300014	9577389	17
13	2792704	290842	3438289	9602125	47	44	2879177	300331	9576552	16
14	2795497	291157	3434563	9601312	46	45	2881963	300648	9575714	15
15	2798290	291473	3430844	9600499	45	46	2884748	300965	9574875	14
16	2801083	291789	3427133	9599684	44	47	2887533	301283	9574035	13
17	2803875	292104	3423429	9598869	43	48	2890318	301600	9573195	12
18	2806667	292420	3419733	9598053	42	49	2893103	301917	9572354	11
19	2809459	292736	3416044	9597236	41	50	2895887	302235	9571512	10
20	2812251	293052	3412362	9596418	40	51	2898671	302552	9570669	9
21	2815043	293368	3408688	9595600	39	52	2901455	302870	9569825	8
22	2817833	293683	3405021	9594781	38	53	2904239	303187	9568981	7
23	2820624	294000	3401361	9593961	37	54	2907022	303505	9568136	6
24	2823415	294316	3397708	9593140	36	55	2909805	303823	9567290	5
25	2826205	294632	3394063	9592318	35	56	2912588	304141	9566443	4
26	2828995	294948	3390424	9591496	34	57	2915371	304458	9565595	3
27	2831785	295264	3386793	9590672	33	58	2918154	304776	9564747	2
28	2834575	295580	3383169	9589848	32	59	2920937	305094	9563898	1
29	2837364	295897	3379553	9589023	31	60	2923717	305412	9563048	0
30	2840153	296213	3375943	9588197	30			305730	9562202	

Deg. 73.

Deg. 73.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

17 Deg.

17 Deg.

/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/
0	.2923717	.305730	3.270852	.9663048	60	.31			.9009832	29	.5363294	3.168380		.9632994	
1	.2926499	.306048	3.267452	.966197	59	32			.9012006	28	.5354518	3.163172		.9635448	
2	.2929280	.306367	3.264059	.9661345	58	33			.9015580	27	.534542	3.161970		.9637974	
3	.2932061	.306685	3.260672	.9660492	57	34			.9018153	26	.5336364	3.158774		.9639664	
4	.2934842	.307003	3.257292	.9659539	56	35			.9020266	25	.5327286	3.155584		.9641397	
5	.2937623	.307321	3.253918	.9658585	55	36			.9022399	24	.5318208	3.152399		.9643107	
6	.2940403	.307640	3.250550	.9657780	54	37			.9024471	23	.5309127	3.149220		.9644807	
7	.2943183	.307958	3.247189	.9656974	53	38			.9026544	22	.5300046	3.146047		.9646501	
8	.2945963	.308277	3.243834	.9656168	52	39			.9028616	21	.5290964	3.142880		.9648194	
9	.2948743	.308595	3.240486	.9655361	51	40			.9030688	20	.5281882	3.139719		.9649882	
10	.2951522	.308914	3.237143	.9654552	50	41			.9032759	19	.5272799	3.136563		.9651569	
11	.2954301	.309231	3.233807	.9653743	49	42			.9034830	18	.5263715	3.133414		.9653254	
12	.2957081	.309551	3.230475	.9652934	48	43			.9036901	17	.5254630	3.130270		.9654938	
13	.2959859	.309870	3.227154	.9652123	47	44			.9038972	16	.5245544	3.127131		.9656621	
14	.2962638	.310189	3.223837	.9651312	46	45			.9041043	15	.5236458	3.124002		.9658303	
15	.2965416	.310508	3.220526	.9650501	45	46			.9043113	14	.5227371	3.120872		.9659984	
16	.2968194	.310827	3.217221	.9649690	44	47			.9045183	13	.5218284	3.117750		.9661664	
17	.2970971	.311146	3.213922	.9648879	43	48			.9047253	12	.5209196	3.114635		.9663344	
18	.2973749	.311465	3.210630	.9648067	42	49			.9049323	11	.5200108	3.111525		.9665023	
19	.2976526	.311784	3.207344	.9647254	41	50			.9051393	10	.5191019	3.108421		.9666701	
20	.2979303	.312103	3.204063	.9646441	40	51			.9053463	9	.5181930	3.105322		.9668379	
21	.2982079	.312422	3.200789	.9645628	39	52			.9055532	8	.5172841	3.102229		.9669956	
22	.2984856	.312742	3.197521	.9644814	38	53			.9057602	7	.5163751	3.099141		.9671532	
23	.2987632	.313061	3.194259	.9643999	37	54			.9059671	6	.5154661	3.096059		.9673107	
24	.2990408	.313381	3.191003	.9643184	36	55			.9061741	5	.5145570	3.092983		.9674681	
25	.2993184	.313700	3.187754	.9642368	35	56			.9063810	4	.5136479	3.089912		.9676255	
26	.2995959	.314020	3.184510	.9641553	34	57			.9065879	3	.5127387	3.086846		.9677828	
27	.2998734	.314339	3.181272	.9640737	33	58			.9067948	2	.5118295	3.083786		.9679400	
28	.3001509	.314659	3.178040	.9639920	32	59			.9069917	1	.5109203	3.080732		.9680971	
29	.3004284	.314979	3.174814	.9639104	31	60			.9071986	0	.5100111	3.077683		.9682542	
30	.3007058	.315298	3.171594	.9638287	30				.9074055					.9684112	

Deg. 72.

Deg. 72.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

18 DEG.

18 DEG.

/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/
0	.3090170	.324919	3.077083	.9510565	60	.3176805	.334918	2.965798	.942313	29
1	.3092336	.325241	3.074640	.9509666	59	.3178563	.335242	2.962916	.9421389	28
2	.3094502	.325563	3.072197	.9508766	58	.3181321	.335566	2.960040	.9419646	27
3	.3096668	.325884	3.069754	.9507865	57	.3184079	.335889	2.957168	.9417903	26
4	.3101234	.326206	3.067311	.9506963	56	.3186836	.336213	2.954301	.9416162	25
5	.3103990	.326528	3.064868	.9506061	55	.3189593	.336537	2.951439	.9414420	24
6	.3106746	.326850	3.062425	.9505157	54	.3192350	.336861	2.948583	.9412678	23
7	.3109502	.327172	3.059982	.9504253	53	.3195106	.337185	2.945731	.9410936	22
8	.3112258	.327494	3.057539	.9503348	52	.3197863	.337509	2.942884	.9409193	21
9	.3115014	.327816	3.055096	.9502443	51	.3200619	.337833	2.940042	.9407450	20
10	.3117770	.328138	3.052653	.9501538	50	.3203376	.338157	2.937205	.9405707	19
11	.3120526	.328461	3.050210	.9500633	49	.3206132	.338481	2.934372	.9403964	18
12	.3123282	.328783	3.047767	.9499728	48	.3208889	.338805	2.931545	.9402221	17
13	.3126038	.329105	3.045324	.9498823	47	.3211645	.339129	2.928722	.9400478	16
14	.3128794	.329428	3.042881	.9497918	46	.3214402	.339454	2.925900	.9398735	15
15	.3131550	.329750	3.040438	.9497013	45	.3217158	.339778	2.923077	.9396992	14
16	.3134306	.330073	3.037995	.9496108	44	.3219915	.340103	2.920254	.9395249	13
17	.3137062	.330395	3.035552	.9495203	43	.3222671	.340427	2.917431	.9393506	12
18	.3139818	.330718	3.033109	.9494298	42	.3225428	.340752	2.914608	.9391763	11
19	.3142574	.331041	3.030666	.9493393	41	.3228184	.341077	2.911785	.9389999	10
20	.3145330	.331363	3.028223	.9492488	40	.3230941	.341401	2.908962	.9388236	9
21	.3148086	.331686	3.025780	.9491583	39	.3233697	.341726	2.906139	.9386473	8
22	.3150842	.332009	3.023337	.9490678	38	.3236454	.342051	2.903316	.9384710	7
23	.3153598	.332332	3.020894	.9489773	37	.3239210	.342376	2.900493	.9382947	6
24	.3156354	.332655	3.018451	.9488868	36	.3241967	.342701	2.897670	.9381184	5
25	.3159110	.332978	3.016008	.9487963	35	.3244723	.343026	2.894847	.9379421	4
26	.3161866	.333301	3.013565	.9487058	34	.3247479	.343351	2.892024	.9377658	3
27	.3164622	.333624	3.011122	.9486153	33	.3250235	.343676	2.889201	.9375895	2
28	.3167378	.333947	3.008679	.9485248	32	.3252991	.344001	2.886378	.9374132	1
29	.3170134	.334270	3.006236	.9484343	31	.3255747	.344326	2.883555	.9372369	0
30	.3172890	.334593	3.003793	.9483438	30	.3258503	.344651	2.880732	.9370606	

DEG. 71.

DEG. 71.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

19 DEG.

19 DEG.

/	SINE.	TANG.	COTANG.	COSINE.	/	/	SINE.	TANG.	COTANG.	COSINE.	/
0	.3255682	.344327	2.904210	.9455186	60	31	.3340810	.354446		.9425444	28
1	.3258432	.344693	2.901468	.9454238	59	32	.3343552	.354773	2.818700	.9424471	29
2	.3261182	.344978	2.898731	.9453290	58	33	.3346293	.355101	2.816100	.9423498	30
3	.3263932	.345264	2.895998	.9452341	57	34	.3349034	.355428	2.813504	.9422525	26
4	.3266681	.345550	2.893270	.9451391	56	35	.3351775	.355756	2.810913	.9421550	27
5	.3269430	.345835	2.890546	.9450441	55	36	.3354516	.356084	2.808326	.9420575	24
6	.3272179	.346121	2.887827	.9449489	54	37	.3357256	.356411	2.805743	.9419598	25
7	.3274928	.346406	2.885113	.9448537	53	38	.3359996	.356739	2.803164	.9418621	22
8	.3277676	.346692	2.882403	.9447584	52	39	.3362735	.357067	2.800590	.9417644	23
9	.3280424	.346978	2.879697	.9446630	51	40	.3365474	.357395	2.798019	.9416665	20
10	.3283172	.347263	2.876987	.9445675	50	41	.3368214	.357723	2.795443	.9415686	19
11	.3285919	.347549	2.874280	.9444720	49	42	.3370953	.358051	2.792871	.9414705	18
12	.3288666	.347834	2.871570	.9443764	48	43	.3373693	.358380	2.790298	.9413724	17
13	.3291413	.348120	2.868862	.9442807	47	44	.3376432	.358708	2.787729	.9412743	16
14	.3294160	.348405	2.866153	.9441849	46	45	.3379171	.359036	2.785155	.9411760	15
15	.3296906	.348691	2.863444	.9440890	45	46	.3381910	.359365	2.782580	.9410777	14
16	.3299653	.348976	2.860735	.9439931	44	47	.3384649	.359693	2.780014	.9409793	13
17	.3302399	.349262	2.858026	.9438971	43	48	.3387388	.360022	2.777444	.9408808	12
18	.3305144	.349547	2.855316	.9438010	42	49	.3390127	.360350	2.774871	.9407822	11
19	.3307889	.349833	2.852607	.9437048	41	50	.3392866	.360679	2.772294	.9406835	10
20	.3310634	.350118	2.850023	.9436085	40	51	.3395605	.361008	2.769719	.9405843	9
21	.3313379	.350403	2.847433	.9435122	39	52	.3398344	.361337	2.767144	.9404850	8
22	.3316123	.350688	2.844843	.9434157	38	53	.3401083	.361666	2.764569	.9403857	7
23	.3318867	.350973	2.842252	.9433192	37	54	.3403822	.361994	2.761994	.9402861	6
24	.3321611	.351258	2.839663	.9432227	36	55	.3406561	.362322	2.759419	.9401861	5
25	.3324355	.351543	2.837071	.9431260	35	56	.3409300	.362650	2.756844	.9400869	4
26	.3327098	.351828	2.834480	.9430293	34	57	.3412039	.362978	2.754269	.9399871	3
27	.3329841	.352113	2.831889	.9429324	33	58	.3414778	.363306	2.751694	.9398871	2
28	.3332584	.352398	2.829291	.9428355	32	59	.3417517	.363634	2.749119	.9397871	1
29	.3335326	.352683	2.826692	.9427386	31	60	.3420256	.363962	2.746544	.9396871	0
30	.3338069	.352968	2.824091	.9426415	30				2.743969	.9395871	

Dsg. 70.

Dsg. 70.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

20 Deg.

20 Deg.

/	/	SINE.	TANG.	COTANG.	COSINE.	/	/	SINE.	TANG.	COTANG.	COSINE.	/	/
0	0	3420201	363070	2747477	9896926	60	31	3504798	374216	2672251	9865703	28	29
1	1	3422835	364289	2747492	9896931	59	32	3507523	374547	2669885	9864683	27	30
2	2	3425468	364659	2747512	9896935	58	33	3510248	374879	2657322	9863462	26	31
3	3	3428100	364938	2747035	9896938	57	34	3512970	375213	2645103	9862241	25	32
4	4	3430733	365258	2737562	9896942	56	35	3515693	375543	2632808	9861018	24	33
5	5	3433365	365618	2735093	9896943	55	36	3518416	375875	2620456	9859846	23	34
6	6	3435997	365948	2732628	9896943	54	37	3521139	376207	2608108	9858671	22	35
7	7	3438629	366277	2730167	9896943	53	38	3523862	376539	2605764	9857521	21	36
8	8	3441260	366607	2727710	9896942	52	39	3526584	376871	2603423	9856468	20	37
9	9	3443891	366937	2725256	9896942	51	40	3529306	377203	2601086	9855440	19	38
10	10	3446521	367268	2722807	9896938	50	41	3532027	377536	2608753	9854423	18	39
11	11	3449152	367598	2720362	9896934	49	42	3534748	377868	2606423	9853412	17	40
12	12	3451782	367928	2717920	9896930	48	43	3537469	378201	2604096	9852401	16	41
13	13	3454411	368258	2715482	9896925	47	44	3540190	378533	2601774	9851392	15	42
14	14	3457041	368589	2713043	9896920	46	45	3542910	378866	2609454	9850381	14	43
15	15	3459670	368919	2710618	9896913	45	46	3545630	379198	2607139	9849370	13	44
16	16	3462300	369250	2708192	9896906	44	47	3548350	379531	2604827	9848359	12	45
17	17	3464928	369580	2705769	9896898	43	48	3551070	379864	2602518	9847347	11	46
18	18	3467557	369911	2703351	9896889	42	49	3553789	380197	2600213	9846336	10	47
19	19	3470185	370242	2700936	9896880	41	50	3556508	380530	2607912	9845324	9	48
20	20	3472812	370572	2698525	9896869	40	51	3559226	380863	2605614	9844311	8	49
21	21	3475440	370903	2696118	9896858	39	52	3561944	381196	2603319	9843300	7	50
22	22	3478067	371234	2693714	9896846	38	53	3564662	381529	2601028	9842289	6	51
23	23	3480694	371565	2691314	9896833	37	54	3567380	381862	2608741	9841277	5	52
24	24	3483320	371896	2688910	9896820	36	55	3570097	382195	2606457	9840266	4	53
25	25	3485947	372227	2686506	9896806	35	56	3572814	382528	2604176	9839255	3	54
26	26	3488573	372558	2684103	9896793	34	57	3575531	382861	2601892	9838244	2	55
27	27	3491198	372889	2681703	9896779	33	58	3578248	383194	2609609	9837233	1	56
28	28	3493824	373221	2679305	9896765	32	59	3580965	383527	2607325	9836222	0	57
29	29	3496449	373552	2676905	9896750	31	60	3583682	383860	2605041	9835211		
30	30	3502074	373884	2674505	9896736	30							

Deg. 69.

Deg. 69.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

21 Deg.

21 Deg.

/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/
0	3583679	384197	2.605089	9335904	60	9667719	394246	2.536483	9303109	28
1	3586395	384531	2.605285	9334761	59	9670425	394582	2.534323	9301242	29
2	3589110	384865	2.605481	9333618	58	9673130	394918	2.532165	9299374	27
3	3591825	385199	2.605676	9332473	57	9675836	395255	2.530011	9297506	26
4	3594540	385533	2.605870	9331328	56	9678541	395591	2.527850	9295638	25
5	3597254	385867	2.606065	9330182	55	9681246	395928	2.525711	9293770	24
6	3600068	386202	2.606259	9329035	54	9683950	396264	2.523565	9291902	23
7	3602882	386536	2.606453	9327889	53	9686655	396601	2.521424	9290034	22
8	3605695	386870	2.606647	9326743	52	9689359	396937	2.519286	9288166	21
9	3608508	387205	2.606840	9325597	51	9692064	397274	2.517150	9286298	20
10	3611321	387539	2.607033	9324450	49	9694768	397611	2.515018	9284430	19
11	3614134	387874	2.607226	9323303	48	9697473	397948	2.512889	9282562	18
12	3616946	388208	2.607419	9322156	47	9700177	398285	2.510762	9280694	17
13	3619758	388543	2.607612	9321009	46	9702882	398622	2.508639	9278826	16
14	3622570	388877	2.607805	9319862	45	9705586	398959	2.506519	9276958	15
15	3625382	389212	2.607998	9318715	44	9708291	399296	2.504402	9275090	14
16	3628194	389546	2.608191	9317568	43	9710995	399633	2.502289	9273222	13
17	3631006	389880	2.608384	9316421	42	9713700	399970	2.500178	9271354	12
18	3633818	390214	2.608577	9315274	41	9716404	400308	2.498070	9269486	11
19	3636630	390548	2.608770	9314127	40	9719109	400646	2.495966	9267618	10
20	3639442	390882	2.608963	9312980	39	9721813	400984	2.493864	9265750	9
21	3642254	391216	2.609156	9311833	38	9724518	401321	2.491766	9263882	8
22	3645066	391550	2.609349	9310686	37	9727222	401659	2.489670	9262014	7
23	3647878	391884	2.609542	9309539	36	9729927	401997	2.487578	9260146	6
24	3650690	392218	2.609735	9308392	35	9732631	402335	2.485488	9258278	5
25	3653502	392552	2.609928	9307245	34	9735336	402673	2.483402	9256410	4
26	3656314	392886	2.610121	9306098	33	9738040	403011	2.481310	9254542	3
27	3659126	393220	2.610314	9304951	32	9740745	403349	2.479228	9252674	2
28	3661938	393554	2.610507	9303804	31	9743449	403687	2.477146	9250806	1
29	3664750	393888	2.610700	9302657	30	9746154	404025	2.475066	9248938	0
30	3667562	394222	2.610893	9301510	29					

Deg. 68.

Deg. 68.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

22 Deg.

22 Deg.

/	/	SINE.	TANG.	COTANG.	COSINE.	/	/	SINE.	TANG.	COTANG.	COSINE.	/
0	1	37.48066	40.4026	2.475086	.9271839	60	31	.9829522	41.4554	2.412228	.9237682	29
1	2	37.48763	40.40564	2.473015	.9270748	59	32	.9832209	41.4805	2.410246	.9236457	28
2	3	37.51450	40.4703	2.470947	.9269658	58	33	.9834895	41.5296	2.408267	.9235132	27
3	4	37.54156	40.5341	2.468881	.9268566	57	34	.9837582	41.5677	2.406280	.9233806	26
4	5	37.56862	40.5980	2.466819	.9267474	56	35	.9840268	41.5918	2.404316	.9232480	25
5	6	37.59567	40.6719	2.464759	.9266380	55	36	.9842953	41.6259	2.402345	.9231154	24
6	7	37.62273	40.6607	2.462703	.9265286	54	37	.9845639	41.6601	2.400377	.9229828	23
7	8	37.64978	40.6735	2.460649	.9264192	53	38	.9848324	41.6942	2.398411	.9228502	22
8	9	37.67683	40.6735	2.458598	.9263096	52	39	.9851008	41.7284	2.396449	.9227176	21
9	10	37.70387	40.7074	2.456551	.9262000	51	40	.9853693	41.7625	2.394488	.9225850	20
10	11	37.73091	40.7514	2.454506	.9260902	50	41	.9856377	41.7967	2.392531	.9224524	19
11	12	37.75795	40.7753	2.452464	.9259805	49	42	.9859060	41.8309	2.390576	.9223198	18
12	13	37.78498	40.8092	2.450425	.9258706	48	43	.9861744	41.8650	2.388625	.9221872	17
13	14	37.81101	40.8431	2.448389	.9257606	47	44	.9864427	41.8992	2.386675	.9220546	16
14	15	37.83794	40.8771	2.446355	.9256506	46	45	.9867110	41.9334	2.384729	.9219220	15
15	16	37.86486	40.9110	2.444325	.9255405	45	46	.9869792	41.9676	2.382785	.9217894	14
16	17	37.89178	40.9450	2.442298	.9254303	44	47	.9872474	42.0019	2.380844	.9216568	13
17	18	37.91870	40.9790	2.440273	.9253201	43	48	.9875156	42.0361	2.378906	.9215242	12
18	19	37.94562	41.0129	2.438251	.9252097	42	49	.9877837	42.0703	2.376970	.9213916	11
19	20	37.97253	41.0469	2.436233	.9250993	41	50	.9880518	42.1046	2.375037	.9212590	10
20	21	37.99944	41.0809	2.434217	.9249888	40	51	.9883199	42.1388	2.373106	.9211264	9
21	22	38.02634	41.1149	2.432204	.9248782	39	52	.9885880	42.1731	2.371179	.9209938	8
22	23	38.05324	41.1489	2.430193	.9247676	38	53	.9888560	42.2073	2.369254	.9208612	7
23	24	38.08014	41.1830	2.428186	.9246568	37	54	.9891240	42.2416	2.367321	.9207286	6
24	25	38.10704	41.2170	2.426181	.9245460	36	55	.9893919	42.2759	2.365391	.9205960	5
25	26	38.13393	41.2510	2.424180	.9244351	35	56	.9896598	42.3102	2.363464	.9204634	4
26	27	38.16082	41.2851	2.422185	.9243242	34	57	.9899277	42.3445	2.361540	.9203308	3
27	28	38.18770	41.3191	2.420188	.9242131	33	58	.9901955	42.3788	2.359618	.9201982	2
28	29	38.21459	41.3532	2.418191	.9241020	32	59	.9904633	42.4131	2.357699	.9200656	1
29	30	38.24147	41.3872	2.416201	.9239908	31	60	.9907311	42.4474	2.355782	.9199330	0
30		38.26834	41.4213	2.414213	.9238795	30						

Deg. 67.

Deg. 67.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

23 Deg.

23 Deg

/	SINE.	TANG.	COTANG.	COSINE.	/	/	SE. NE.	TANG.	COTANG.	COSINE.	/
0	3907311	424474	2-355852	9250549	59	31	3900135	435158	2-298014	9168440	29
1	3909980	424818	2-353948	9203912	60	32	3892285	435504	2-296188	9168270	28
2	3912690	425161	2-352046	9202774	58	33	3894502	435850	2-294325	9171718	27
3	3915343	425505	2-350148	9201635	57	34	3896188	436196	2-292454	9169305	26
4	3918019	425848	2-348251	9200496	56	35	3897825	436542	2-290575	9166931	25
5	3920695	426192	2-346358	9199356	55	36	3899460	436889	2-288699	9164562	24
6	3923371	426536	2-344467	9198215	54	37	3901095	437235	2-286824	9162192	23
7	3926047	426880	2-342578	9197073	53	38	3902730	437582	2-284947	9159820	22
8	3928722	427223	2-340682	9195931	52	39	3904365	437928	2-283075	9157456	21
9	3931397	427568	2-338789	9194788	51	40	3906000	438275	2-281198	9155093	20
10	3934071	427912	2-336898	9193644	50	41	3907635	438622	2-279322	9152730	19
11	3936745	428256	2-335000	9192499	49	42	3909270	438969	2-277445	9150367	18
12	3939419	428600	2-333104	9191353	48	43	3910905	439316	2-275569	9148004	17
13	3942093	428944	2-331201	9190207	47	44	3912540	439663	2-273692	9145641	16
14	3944767	429289	2-329293	9189060	46	45	3914175	440010	2-271816	9143278	15
15	3947439	429633	2-327383	9187912	45	46	3915810	440357	2-269940	9140915	14
16	3950111	429978	2-325469	9186763	44	47	3917445	440705	2-268064	9138552	13
17	3952783	430323	2-323554	9185614	43	48	3919080	441052	2-266188	9136189	12
18	3955455	430668	2-321640	9184464	42	49	3920715	441400	2-264312	9133826	11
19	3958127	431012	2-320116	9183313	41	50	3922350	441747	2-262436	9131463	10
20	3960798	431357	2-318260	9182161	40	51	3923985	442095	2-260560	9129100	9
21	3963468	431703	2-316407	9181009	39	52	3925620	442443	2-258684	9126737	8
22	3966139	432048	2-314557	9179855	38	53	3927255	442791	2-256808	9124374	7
23	3968809	432393	2-312709	9178701	37	54	3928890	443139	2-254932	9122011	6
24	3971479	432738	2-310863	9177546	36	55	3930525	443487	2-253056	9119648	5
25	3974148	433084	2-309020	9176391	35	56	3932160	443835	2-251180	9117285	4
26	3976818	433429	2-307180	9175234	34	57	3933795	444183	2-249304	9114922	3
27	3979486	433775	2-305342	9174077	33	58	3935430	444531	2-247428	9112559	2
28	3982155	434120	2-303506	9172919	32	59	3937065	444880	2-245552	9110196	1
29	3984823	434466	2-301673	9171760	31	60	3938700	445228	2-243676	9107833	0
30	3987491	434812	2-299842	9170601	30						

Deg. 66.

Deg. 66

NATURAL SINES AND TANGENTS TO A RADIUS 1.

24 Deg.

24 Deg.

/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/
0	.0000000	.0000000	∞	1.0000000	30	.5000000	1.0000000	1.0000000	.8660254	29
1	.0001746	.0003492	286.45380	.9998254	31	.5091753	1.0167439	0.9832561	.8632094	28
2	.0003492	.0006984	143.22690	.9996508	32	.5183506	1.0334878	0.9665121	.8603934	27
3	.0005236	.0010476	95.49150	.9994762	33	.5275259	1.0502317	0.9497680	.8575774	26
4	.0006984	.0013968	71.61900	.9993016	34	.5367012	1.0669756	0.9330239	.8547614	25
5	.0008728	.0017460	57.74650	.9991270	35	.5458765	1.0837195	0.9162798	.8519454	24
6	.0010476	.0020952	43.87400	.9989524	36	.5550518	1.1004634	0.8995357	.8491294	23
7	.0012220	.0024444	35.71700	.9987778	37	.5642271	1.1172073	0.8827916	.8463134	22
8	.0013968	.0027936	29.65400	.9986032	38	.5734024	1.1339512	0.8660475	.8434974	21
9	.0015712	.0031428	25.71700	.9984286	39	.5825777	1.1506951	0.8493014	.8406814	20
10	.0017460	.0034920	22.38000	.9982540	40	.5917530	1.1674390	0.8325553	.8378654	19
11	.0019204	.0038412	19.65400	.9980794	41	.6009283	1.1841829	0.8158092	.8350494	18
12	.0020952	.0041904	17.32700	.9979048	42	.6101036	1.2009268	0.7990631	.8322334	17
13	.0022696	.0045396	15.38000	.9977302	43	.6192789	1.2176707	0.7823170	.8294174	16
14	.0024440	.0048888	13.71700	.9975556	44	.6284542	1.2344146	0.7655709	.8266014	15
15	.0026184	.0052380	12.32700	.9973810	45	.6376295	1.2511585	0.7488248	.8237854	14
16	.0027928	.0055872	11.17400	.9972064	46	.6468048	1.2679024	0.7320787	.8209694	13
17	.0029672	.0059364	10.21700	.9970318	47	.6559801	1.2846463	0.7153326	.8181534	12
18	.0031416	.0062856	9.41400	.9968572	48	.6651554	1.3013902	0.6985865	.8153374	11
19	.0033160	.0066348	8.74700	.9966826	49	.6743307	1.3181341	0.6818404	.8125214	10
20	.0034904	.0069840	8.18000	.9965080	50	.6835060	1.3348780	0.6650943	.8097054	9
21	.0036648	.0073332	7.69400	.9963334	51	.6926813	1.3516219	0.6483482	.8068894	8
22	.0038392	.0076824	7.26700	.9961588	52	.7018566	1.3683658	0.6316021	.8040734	7
23	.0040136	.0080316	6.89000	.9959842	53	.7110319	1.3851097	0.6148560	.8012574	6
24	.0041880	.0083808	6.56300	.9958096	54	.7202072	1.4018536	0.5981099	.7984414	5
25	.0043624	.0087300	6.28600	.9956350	55	.7293825	1.4185975	0.5813638	.7956254	4
26	.0045368	.0090792	6.05900	.9954604	56	.7385578	1.4353414	0.5646177	.7928094	3
27	.0047112	.0094284	5.88200	.9952858	57	.7477331	1.4520853	0.5478716	.7900034	2
28	.0048856	.0097776	5.74500	.9951112	58	.7569084	1.4688292	0.5311258	.7871874	1
29	.0050600	.0101268	5.64800	.9949366	59	.7660837	1.4855731	0.5143797	.7843714	0
30	.0052344	.0104760	5.58100	.9947620	60	.7752590	1.5023170	0.4976336	.7815554	

Deg. 65.

Deg. 65.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

25 DEG.

25 DEG.

/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/
0	.4226183	.460307	2.144506	.9063078	60	.4307736	.477332	2.094975	.9024600	29
1	.4226819	.460661	2.142879	.9061848	59	.4310286	.477089	2.093408	.9023347	28
2	.4227455	.461016	2.141253	.9060618	58	.4312836	.476847	2.091843	.9022092	27
3	.4228090	.461370	2.139630	.9059386	57	.4315386	.476604	2.090280	.9020838	26
4	.4228725	.461725	2.138008	.9058154	56	.4317936	.476362	2.088720	.9019582	25
5	.4229360	.462079	2.136389	.9056922	55	.4320486	.476119	2.087161	.9018325	24
6	.4229995	.462434	2.134771	.9055688	54	.4323036	.475877	2.085603	.9017068	23
7	.4230630	.462789	2.133155	.9054454	53	.4325586	.475635	2.084048	.9015810	22
8	.4231265	.463143	2.131542	.9053219	52	.4328136	.475393	2.082495	.9014551	21
9	.4231900	.463498	2.129930	.9051983	51	.4330686	.475151	2.080943	.9013292	20
10	.4232535	.463853	2.128321	.9050746	50	.4333236	.474909	2.079394	.9012031	19
11	.4233170	.464208	2.126713	.9049509	49	.4335786	.474667	2.077846	.9010770	18
12	.4233805	.464563	2.125108	.9048272	48	.4338336	.474425	2.076296	.9009508	17
13	.4234440	.464918	2.123504	.9047032	47	.4340886	.474183	2.074756	.9008246	16
14	.4235075	.465273	2.121903	.9045792	46	.4343436	.473941	2.073214	.9006982	15
15	.4235710	.465628	2.120303	.9044551	45	.4345986	.473699	2.071674	.9005718	14
16	.4236345	.465983	2.118705	.9043310	44	.4348536	.473457	2.070135	.9004453	13
17	.4236980	.466338	2.117110	.9042068	43	.4351086	.473215	2.068599	.9003188	12
18	.4237615	.466693	2.115516	.9040825	42	.4353636	.472973	2.067064	.9001921	11
19	.4238250	.467048	2.113924	.9039582	41	.4356186	.472731	2.065531	.9000654	10
20	.4238885	.467403	2.112334	.9038338	40	.4358736	.472489	2.064000	.8999386	9
21	.4239520	.467758	2.110747	.9037093	39	.4361286	.472247	2.062471	.8998117	8
22	.4240155	.468113	2.109161	.9035847	38	.4363836	.472005	2.060944	.8996848	7
23	.4240790	.468468	2.107577	.9034600	37	.4366386	.471763	2.059418	.8995578	6
24	.4241425	.468823	2.105995	.9033353	36	.4368936	.471521	2.057895	.8994307	5
25	.4242060	.469178	2.104415	.9032105	35	.4371486	.471279	2.056373	.8993035	4
26	.4242695	.469533	2.102836	.9030856	34	.4374036	.471037	2.054853	.8991763	3
27	.4243330	.469888	2.101260	.9029606	33	.4376586	.470795	2.053334	.8990490	2
28	.4243965	.470243	2.099686	.9028358	32	.4379136	.470553	2.051818	.8989216	1
29	.4244600	.470598	2.098114	.9027105	31	.4381686	.470311	2.050303	.8987940	0
30	.4245235	.470953	2.096543	.9025853	30					

DEG. 64.

DEG. 64.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

25 DEG.

26 DEG.

/	SINE.	TANG.	COTANG.	COSINE.	1/	/	SINE.	TANG.	COTANG.	COSINE.	/
0	.43303711	.487732	2.0650903	.8987940	60	31	.4465851	.498044	2.004229	.8948045	29
1	.43363326	.488092	2.048701	.8986365	59	32	.4467184	.498308	2.002771	.8946746	28
2	.43423840	.488453	2.047280	.8984839	58	33	.4468786	.498671	2.001314	.8945446	27
3	.4348513	.488813	2.045770	.8983412	57	34	.4470591	.500038	1.999805	.8944146	26
4	.4354719	.489173	2.044263	.8982034	56	35	.4472544	.500762	1.998353	.8942846	25
5	.4360979	.489534	2.042757	.8980715	55	36	.4474691	.501626	1.996905	.8941546	24
6	.4367292	.489894	2.041254	.8979456	54	37	.4476992	.502612	1.995463	.8940246	23
7	.4373658	.490255	2.039751	.8978257	53	38	.4479392	.503728	1.994029	.8938946	22
8	.4400204	.490616	2.038251	.8977115	52	39	.4481892	.504969	1.992608	.8937646	21
9	.4407227	.490977	2.036753	.8976033	51	40	.4484392	.506328	1.991193	.8936346	20
10	.4409838	.491338	2.035256	.8975011	50	41	.4486892	.507806	1.989778	.8935046	19
11	.4412448	.491699	2.033761	.8974049	49	42	.4489392	.509306	1.988363	.8933746	18
12	.4415059	.492061	2.032268	.8973148	48	43	.4491892	.510828	1.986948	.8932446	17
13	.4417668	.492422	2.030776	.8972299	47	44	.4494392	.512372	1.985533	.8931146	16
14	.4420278	.492783	2.029287	.8971461	46	45	.4496892	.513938	1.984118	.8929846	15
15	.4422887	.493145	2.027799	.8970634	45	46	.4499392	.515526	1.982703	.8928546	14
16	.4425496	.493507	2.026313	.8969817	44	47	.4501892	.517136	1.981288	.8927246	13
17	.4428104	.493868	2.024828	.8969013	43	48	.4504392	.518768	1.979873	.8925946	12
18	.4430712	.494230	2.023346	.8968219	42	49	.4506892	.520422	1.978458	.8924646	11
19	.4433319	.494592	2.021865	.8967434	41	50	.4509392	.522098	1.977043	.8923346	10
20	.4435927	.494954	2.020386	.8966658	40	51	.4511892	.523796	1.975628	.8922046	9
21	.4438534	.495317	2.018908	.8965894	39	52	.4514392	.525516	1.974213	.8920746	8
22	.4441140	.495679	2.017433	.8965139	38	53	.4516892	.527258	1.972798	.8919446	7
23	.4443746	.496040	2.015959	.8964391	37	54	.4519392	.529022	1.971383	.8918146	6
24	.4446352	.496404	2.014486	.8963646	36	55	.4521892	.530808	1.969968	.8916846	5
25	.4448957	.496766	2.013016	.8962912	35	56	.4524392	.532616	1.968553	.8915546	4
26	.4451562	.497129	2.011547	.8962188	34	57	.4526892	.534446	1.967138	.8914246	3
27	.4454167	.497495	2.010080	.8961473	33	58	.4529392	.536298	1.965723	.8912946	2
28	.4456771	.497855	2.008615	.8960768	32	59	.4531892	.538172	1.964308	.8911646	1
29	.4459375	.498218	2.007151	.8960071	31	60	.4534392	.540068	1.962893	.8910346	0
30	.4461978	.498581	2.005689	.8959384	30		.4536892	.541986	1.961478	.8909046	

DEG. 63.

DEG. 63.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

27 DEG.

27 DEG.

/	SINE.	TANG.	COTANG.	COSINE.	/	/	SINE.	TANG.	COTANG.	COSINE.	/	/
0	.4538945	.500825	1.962010	.8910065	60	31	.4620066	.520935	1.919018	.8898765	29	29
1	.4542437	.500891	1.961200	.890744	59	32	.4622546	.521206	1.918256	.8897420	28	28
2	.4545988	.501025	1.959791	.8904723	58	33	.4625225	.521676	1.916896	.8896075	27	27
3	.4549579	.5010625	1.958383	.8901600	57	34	.462804	.522246	1.915537	.8894730	26	26
4	.4553269	.5010991	1.956978	.8900477	56	35	.4630882	.522817	1.914179	.8893383	25	25
5	.4556985	.5011358	1.955573	.8900452	55	36	.4633860	.523417	1.912823	.8892036	24	24
6	.4560749	.5011725	1.954171	.8900428	54	37	.4636889	.524017	1.911469	.8890688	23	23
7	.4564564	.5012093	1.952770	.8900403	53	38	.4639915	.524617	1.910116	.8889339	22	22
8	.4568430	.5012460	1.951371	.8900376	52	39	.4643029	.525217	1.908764	.8887989	21	21
9	.4572346	.5012827	1.949973	.8900349	51	40	.4646185	.525817	1.907414	.8886639	20	20
10	.4576312	.5013193	1.948578	.8900322	50	41	.4649389	.526417	1.906066	.8885288	19	19
11	.4580328	.5013559	1.947182	.8900294	49	42	.4652641	.527017	1.904719	.8883936	18	18
12	.4584394	.5013923	1.945789	.8900264	48	43	.4655941	.527617	1.903373	.8882584	17	17
13	.4588510	.5014288	1.944398	.8900233	47	44	.4659289	.528217	1.902029	.8881230	16	16
14	.4592676	.5014653	1.943008	.8900200	46	45	.4662685	.528817	1.900687	.8879876	15	15
15	.4596892	.5015017	1.941620	.8900165	45	46	.4666129	.529417	1.899346	.8878522	14	14
16	.4601158	.5015380	1.940233	.8900129	44	47	.4669621	.530017	1.898006	.8877166	13	13
17	.4605474	.5015742	1.938848	.8900092	43	48	.4673161	.530617	1.896668	.8875810	12	12
18	.4609840	.5016103	1.937464	.8900054	42	49	.4676749	.531217	1.895332	.8874453	11	11
19	.4614256	.5016464	1.936082	.8900015	41	50	.4680385	.531817	1.893997	.8873095	10	10
20	.4618722	.5016825	1.934702	.8900000	40	51	.4684069	.532417	1.892663	.8871736	9	9
21	.4623238	.5017185	1.933323	.8900000	39	52	.4687801	.533017	1.891331	.8870377	8	8
22	.4627804	.5017544	1.931945	.8900000	38	53	.4691581	.533617	1.890000	.8869017	7	7
23	.4632420	.5017902	1.930569	.8900000	37	54	.4695409	.534217	1.888668	.8867656	6	6
24	.4637086	.5018259	1.929195	.8900000	36	55	.4699285	.534817	1.887334	.8866295	5	5
25	.4641802	.5018615	1.927822	.8900000	35	56	.4703209	.535417	1.886000	.8864933	4	4
26	.4646568	.5018970	1.926451	.8900000	34	57	.4707181	.536017	1.884666	.8863570	3	3
27	.4651384	.5019324	1.925081	.8900000	33	58	.4711201	.536617	1.883332	.8862206	2	2
28	.4656250	.5019677	1.923713	.8900000	32	59	.4715279	.537217	1.882000	.8860841	1	1
29	.4661166	.5020029	1.922347	.8900000	31	60	.4719415	.537817	1.880666	.8859476	0	0
30	.4666132	.5020382	1.920982	.8900000	30							

Deg. 62.

Deg. 62.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

28 Deg.

28 Deg.

/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/
0	.4694716	.531709	1.880726	.8529476	60	.474144	.543332	1.840494	.8786783	29
1	.4698284	.532092	1.879407	.8528110	59	.4747600	.543709	1.839218	.8785394	28
2	.4699852	.532455	1.878089	.8526743	58	.4753755	.544086	1.837944	.8784004	27
3	.4702419	.532829	1.876773	.8525376	57	.4759910	.544463	1.836671	.8782613	26
4	.4704986	.533202	1.875458	.8524007	56	.4766065	.544840	1.835399	.8781222	25
5	.4707553	.533576	1.874145	.8522638	55	.4772220	.545217	1.834126	.8779830	24
6	.4710119	.533950	1.872833	.8521269	54	.4778375	.545595	1.832851	.8778437	23
7	.4712685	.534324	1.871523	.8519908	53	.4784530	.545972	1.831583	.8777043	22
8	.4715250	.534698	1.870214	.8518547	52	.4790685	.546350	1.830327	.8775649	21
9	.4717815	.535072	1.868906	.8517185	51	.4796840	.546728	1.829062	.8774254	20
10	.4720380	.535446	1.867600	.8515823	50	.4802995	.547106	1.827799	.8772858	19
11	.4722944	.535820	1.866295	.8514460	49	.4809150	.547484	1.826537	.8771462	18
12	.4725508	.536195	1.864992	.8513095	48	.4815305	.547862	1.825276	.8770064	17
13	.4728071	.536569	1.863690	.8511730	47	.4821460	.548240	1.824017	.8768666	16
14	.4730634	.536944	1.862389	.8510364	46	.4827615	.548618	1.822759	.8767268	15
15	.4733197	.537319	1.861090	.8508997	45	.4833770	.548997	1.821502	.8765868	14
16	.4735759	.537694	1.859792	.8507630	44	.4839925	.549375	1.820247	.8764468	13
17	.4738321	.538069	1.858496	.8506263	43	.4846080	.549754	1.818993	.8763067	12
18	.4740882	.538444	1.857201	.8504894	42	.4852235	.550133	1.817740	.8761663	11
19	.4743443	.538819	1.855908	.8503524	41	.4858390	.550512	1.816489	.8760263	10
20	.4746004	.539195	1.854615	.8502154	40	.4864545	.550891	1.815239	.8758859	9
21	.4748564	.539570	1.853325	.8500783	39	.4870700	.551270	1.813990	.8757455	8
22	.4751124	.539946	1.852035	.8499413	38	.4876855	.551650	1.812743	.8756051	7
23	.4753683	.540322	1.850747	.8498042	37	.4883010	.552029	1.811496	.8754645	6
24	.4756242	.540698	1.849461	.8496671	36	.4889165	.552409	1.810252	.8753239	5
25	.4758801	.541074	1.848176	.8495300	35	.4895320	.552789	1.809008	.8751832	4
26	.4761359	.541450	1.846892	.8493929	34	.4901475	.553168	1.807765	.8750425	3
27	.4763917	.541826	1.845608	.8492558	33	.4907630	.553548	1.806525	.8749016	2
28	.4766474	.542202	1.844328	.8491187	32	.4913785	.553928	1.805286	.8747607	1
29	.4769031	.542579	1.843049	.8489816	31	.4919940	.554309	1.804047	.8746197	0
30	.4771588	.542955	1.841770	.8488445	30					

Deg. 61.

Deg. 61.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

29 DEG.

29 DEG.

/	/	SINE.	TANG.	COTANG.	COSINE.	/	/	SINE.	TANG.	COTANG.	COSINE.	/	/
0	1	.4848096	.554309	1.804047	.8746197	60	31	.4922767	.566156	1.766295	.8702124	28	29
1	2	.4850640	.554689	1.802810	.8744786	59	32	.4925298	.566541	1.765097	.8700691	29	30
2	3	.4853184	.555069	1.801575	.8743375	58	33	.4937829	.566925	1.763900	.8699256	36	37
3	4	.4855727	.555450	1.800340	.8741963	57	34	.4935359	.567309	1.762705	.8697821	37	38
4	5	.4858270	.555831	1.799107	.8740550	56	35	.4932889	.567694	1.761511	.8696386	38	39
5	6	.4860812	.556211	1.797875	.8739137	55	36	.4930419	.568079	1.760318	.8694949	39	40
6	7	.4863354	.556592	1.796645	.8737722	54	37	.4927949	.568463	1.759126	.8693512	40	41
7	8	.4865895	.556973	1.795416	.8736307	53	38	.4925476	.568848	1.757936	.8692074	41	42
8	9	.4868436	.557355	1.794188	.8734891	52	39	.4923005	.569233	1.756747	.8690636	42	43
9	10	.4870977	.557736	1.792961	.8733475	51	40	.4920532	.569619	1.755559	.8689196	43	44
10	11	.4873517	.558117	1.791735	.8732058	50	41	.4918060	.570004	1.754372	.8687756	44	45
11	12	.4876057	.558499	1.790512	.8730640	49	42	.4915587	.570389	1.753186	.8686315	45	46
12	13	.4878597	.558881	1.789289	.8729221	48	43	.4913113	.570775	1.752002	.8684874	46	47
13	14	.4881136	.559262	1.788067	.8727801	47	44	.4910639	.571161	1.750819	.8683431	47	48
14	15	.4883674	.559644	1.786847	.8726381	46	45	.4908165	.571547	1.749637	.8681988	48	49
15	16	.4886212	.560026	1.785628	.8724960	45	46	.4905690	.571933	1.748456	.8680544	49	50
16	17	.4888750	.560409	1.784410	.8723538	44	47	.4903215	.572319	1.747276	.8679100	50	51
17	18	.4891288	.560791	1.783194	.8722116	43	48	.4900740	.572705	1.746098	.8677655	51	52
18	19	.4893825	.561173	1.781979	.8720693	42	49	.4898264	.573091	1.744921	.8676209	52	53
19	20	.4896361	.561556	1.780765	.8719269	41	50	.4895787	.573478	1.743745	.8674762	53	54
20	21	.4898897	.561939	1.779552	.8717844	40	51	.4893310	.573864	1.742570	.8673314	54	55
21	22	.4901433	.562321	1.778340	.8716419	39	52	.4890833	.574251	1.741396	.8671866	55	56
22	23	.4903968	.562704	1.777130	.8714993	38	53	.4888355	.574638	1.740224	.8670417	56	57
23	24	.4906503	.563087	1.775921	.8713566	37	54	.4885877	.575025	1.739053	.8668967	57	58
24	25	.4909038	.563471	1.774714	.8712138	36	55	.4883399	.575412	1.737883	.8667517	58	59
25	26	.4911572	.563854	1.773507	.8710710	35	56	.4880920	.575799	1.736714	.8666066	59	60
26	27	.4914105	.564237	1.772302	.8709281	34	57	.4878441	.576187	1.735546	.8664614	60	61
27	28	.4916638	.564621	1.771098	.8707851	33	58	.4875962	.576574	1.734380	.8663161	61	62
28	29	.4919171	.565005	1.769895	.8706420	32	59	.4873483	.576962	1.733214	.8661708	62	63
29	30	.4921704	.565388	1.768694	.8704989	31	60	.4871004	.577350	1.732050	.8660254	63	64
30		.4924236	.565772	1.767494	.8703557	30							

Deg. 60.

Deg. 60.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

30 Deg.

30 Deg.

/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/
0	.5000000	.577350	1.732050	.8660254	60	.917356	1.966334	1.038469	.1961261	29
1	.5002173	.577738	1.730887	.8658799	59	.916987	1.965288	1.039436	.1962837	28
2	.5004347	.578126	1.729726	.8657344	58	.916618	1.964241	1.040503	.1961413	27
3	.5006521	.578514	1.728565	.8655887	57	.916249	1.963195	1.041570	.1960000	26
4	.5008695	.578902	1.727405	.8654430	56	.915880	1.962149	1.042637	.1958587	25
5	.5010869	.579291	1.726244	.8652973	55	.915511	1.961103	1.043704	.1957174	24
6	.5013043	.579679	1.725084	.8651514	54	.915142	1.960057	1.044771	.1955761	23
7	.5015217	.580067	1.723924	.8650055	53	.914773	1.959011	1.045838	.1954348	22
8	.5017391	.580455	1.722764	.8648596	52	.914404	1.957965	1.046905	.1952935	21
9	.5019565	.580843	1.721604	.8647137	51	.914035	1.956919	1.047972	.1951522	20
10	.5021739	.581231	1.720443	.8645678	50	.913666	1.955873	1.049039	.1950109	19
11	.5023913	.581619	1.719283	.8644219	49	.913297	1.954827	1.050106	.1948696	18
12	.5026087	.582007	1.718122	.8642760	48	.912928	1.953781	1.051173	.1947283	17
13	.5028261	.582395	1.716962	.8641301	47	.912559	1.952735	1.052240	.1945870	16
14	.5030435	.582783	1.715801	.8639842	46	.912190	1.951689	1.053307	.1944457	15
15	.5032609	.583171	1.714641	.8638383	45	.911821	1.950643	1.054374	.1943044	14
16	.5034783	.583559	1.713480	.8636924	44	.911452	1.949597	1.055441	.1941631	13
17	.5036957	.583947	1.712320	.8635465	43	.911083	1.948551	1.056508	.1940218	12
18	.5039131	.584335	1.711159	.8634006	42	.910714	1.947505	1.057575	.1938805	11
19	.5041305	.584723	1.710000	.8632547	41	.910345	1.946459	1.058642	.1937392	10
20	.5043479	.585111	1.708840	.8631088	40	.909976	1.945413	1.059709	.1935979	9
21	.5045653	.585499	1.707680	.8629629	39	.909607	1.944367	1.060776	.1934566	8
22	.5047827	.585887	1.706520	.8628170	38	.909238	1.943321	1.061843	.1933153	7
23	.5050001	.586275	1.705360	.8626711	37	.908869	1.942275	1.062910	.1931740	6
24	.5052175	.586663	1.704200	.8625252	36	.908500	1.941229	1.063977	.1930327	5
25	.5054349	.587051	1.703040	.8623793	35	.908131	1.940183	1.065044	.1928914	4
26	.5056523	.587439	1.701880	.8622334	34	.907762	1.939137	1.066111	.1927501	3
27	.5058697	.587827	1.700720	.8620875	33	.907393	1.938091	1.067178	.1926088	2
28	.5060871	.588215	1.699560	.8619416	32	.907024	1.937045	1.068245	.1924675	1
29	.5063045	.588603	1.698400	.8617957	31	.906655	1.936000	1.069312	.1923262	0
30	.5065219	.588991	1.697240	.8616498	30	.906286	1.934954	1.070379	.1921849	

Deg. 59.

Deg. 59.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

31 Deg.

31 Deg.

/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/
0	·5150381	·0000000	1·664279	·8571673	60	·31	·527466	·613201	1·630786	29
1	·5152874	·001256	1·663183	·8570174	59	32	·5229445	·613001	1·629722	28
2	·5155367	·002512	1·662088	·8568675	58	33	·5234244	·614001	1·628559	27
3	·5157859	·003769	1·660994	·8567175	57	34	·5239033	·614803	1·627597	26
4	·5160351	·005024	1·659901	·8565674	56	35	·5243822	·615204	1·626536	25
5	·5162842	·006281	1·658809	·8564173	55	36	·5248611	·615605	1·625476	24
6	·5165333	·007538	1·657718	·8562671	54	37	·5253400	·616006	1·624417	23
7	·5167824	·008795	1·656629	·8561168	53	38	·5258189	·616407	·8514219	22
8	·5170314	·010052	1·655540	·8559664	52	39	·5262978	·616809	·851167	21
9	·5172804	·011309	1·654452	·8558160	51	40	·5267767	·617210	·8509639	20
10	·5175293	·012566	1·653366	·8556655	50	41	·5272556	·617612	·8508111	19
11	·5177782	·013823	1·652280	·8555149	49	42	·5277345	·618014	·8506582	18
12	·5180270	·015080	1·651196	·8553643	48	43	·5282134	·618416	·8505053	17
13	·5182758	·016337	1·650112	·8552135	47	44	·5286923	·618818	·8503522	16
14	·5185246	·017594	1·649030	·8550627	46	45	·5291712	·619221	·8501991	15
15	·5187733	·018851	1·647949	·8549119	45	46	·5296501	·619623	·8500459	14
16	·5190219	·020108	1·646868	·8547609	44	47	·5301290	·620025	·8498927	13
17	·5192705	·021365	1·645789	·8546099	43	48	·5306079	·620429	·8497394	12
18	·5195191	·022622	1·644711	·8544588	42	49	·5310868	·620832	·8495860	11
19	·5197676	·023879	1·643633	·8543077	41	50	·5315657	·621235	·8494325	10
20	·5200161	·025136	1·642557	·8541564	40	51	·5320446	·621638	·8492790	9
21	·5202646	·026393	1·641482	·8540051	39	52	·5325235	·622041	·8491254	8
22	·5205131	·027650	1·640408	·8538538	38	53	·5330024	·622445	·8489717	7
23	·5207616	·028907	1·639335	·8537023	37	54	·5334813	·622848	·8488179	6
24	·5210101	·030164	1·638263	·8535508	36	55	·5339602	·623252	·8486641	5
25	·5212586	·031421	1·637191	·8533992	35	56	·5344391	·623656	·8485102	4
26	·5215071	·032678	1·636121	·8532475	34	57	·5349180	·624060	·8483562	3
27	·5217556	·033935	1·635052	·8530958	33	58	·5353969	·624465	·8482022	2
28	·5220041	·035192	1·633984	·8529440	32	59	·5358758	·624869	·8480481	1
29	·5222526	·036449	1·632917	·8527921	31	60	·5363547	·625273		0
30	·5225011	·037706	1·631851	·8526402	30					

Deg. 58.

Deg. 58

NATURAL SINES AND TANGENTS TO A RADIUS 1.

32 DEG.

32 DEG.

/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/
0	.5299193	.624869	1.600334	.8480481	60	.5375449	.637479	1.568078	.8432351	29
1	.5304169	.625273	1.599299	.8478939	59	.5380902	.637888	1.567672	.8430787	28
2	.5309125	.625678	1.598264	.8477397	58	.5386834	.638297	1.566666	.8429222	27
3	.5314061	.626083	1.597231	.8475853	57	.5392806	.638707	1.565662	.8427657	26
4	.5319007	.626488	1.596198	.8474309	56	.5398827	.639116	1.564659	.8426091	25
5	.5323951	.626893	1.595167	.8472765	55	.5404887	.639526	1.563656	.8424524	24
6	.5328902	.627298	1.594136	.8471219	54	.5410901	.639936	1.562654	.8422956	23
7	.5333851	.627704	1.593107	.8469673	53	.5416938	.640346	1.561654	.8421388	22
8	.5338813	.628109	1.592078	.8468126	52	.5422998	.640756	1.560654	.8419819	21
9	.5343776	.628515	1.591050	.8466579	51	.5429065	.641167	1.559655	.8418249	20
10	.5348739	.628921	1.590023	.8465030	50	.5435137	.641577	1.558657	.8416679	19
11	.5353691	.629327	1.588997	.8463481	49	.5441215	.641988	1.557660	.8415108	18
12	.5358643	.629733	1.587973	.8461932	48	.5447298	.642399	1.556663	.8413536	17
13	.5363595	.630139	1.586949	.8460381	47	.5453387	.642810	1.555668	.8411963	16
14	.5368545	.630546	1.585926	.8458830	46	.5459474	.643221	1.554674	.8410390	15
15	.5373495	.630953	1.584904	.8457278	45	.5465562	.643632	1.553680	.8408816	14
16	.5378445	.631359	1.583883	.8455726	44	.5471652	.644044	1.552688	.8407241	13
17	.5383395	.631766	1.582862	.8454172	43	.5477747	.644456	1.551696	.8405666	12
18	.5388345	.632173	1.581843	.8452618	42	.5483847	.644867	1.550705	.8404090	11
19	.5393295	.632581	1.580825	.8451064	41	.5489952	.645279	1.549715	.8402513	10
20	.5398245	.632988	1.579807	.8449508	40	.5496061	.645691	1.548726	.8400936	9
21	.5403195	.633395	1.578791	.8447952	39	.5502175	.646104	1.547738	.8399357	8
22	.5408145	.633803	1.577776	.8446395	38	.5508292	.646516	1.546751	.8397778	7
23	.5413095	.634211	1.576761	.8444838	37	.5514415	.646929	1.545764	.8396199	6
24	.5418045	.634619	1.575747	.8443279	36	.5520541	.647341	1.544779	.8394618	5
25	.5422995	.635027	1.574735	.8441720	35	.5526672	.647754	1.543794	.8393037	4
26	.5427945	.635435	1.573723	.8440161	34	.5532809	.648167	1.542810	.8391455	3
27	.5432895	.635844	1.572712	.8438600	33	.5538951	.648580	1.541828	.8389873	2
28	.5437845	.636252	1.571702	.8437039	32	.5545098	.648994	1.540846	.8388290	1
29	.5442795	.636661	1.570693	.8435477	31	.5551250	.649407	1.539865	.8386706	0
30	.5447745	.637070	1.569685	.8433914	30					

DEG. 57

DEG. 57.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

33 Deg.

33 Deg.

/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/
0	.5446390	.6149407	1.5598865	.8386706	60	.31	.62204	1.609880	.8337252	29
1	.5448380	.6149821	1.5598884	.8386121	59	32	.62222	1.608927	.8335946	28
2	.5451269	.6150235	1.5599005	.8385336	58	33	.62240	1.607974	.8334038	27
3	.5454707	.6150649	1.5599227	.8384360	57	34	.62258	1.607022	.8332340	26
4	.5458145	.6151063	1.5599449	.8383160	56	35	.62276	1.606071	.8330822	25
5	.5461583	.6151477	1.5599671	.8381775	55	36	.62294	1.605121	.8329422	24
6	.5465020	.6151891	1.5599894	.8380250	54	37	.62312	1.604171	.8327802	23
7	.5468456	.6152305	1.5600116	.8378585	53	38	.62330	1.603222	.8325991	22
8	.5471892	.6152719	1.5600338	.8376771	52	39	.62348	1.602275	.8324380	21
9	.5475328	.6153133	1.5600560	.8374818	51	40	.62366	1.601328	.8322768	20
10	.5478764	.6153547	1.5600782	.8372825	50	41	.62384	1.600382	.8321155	19
11	.5482199	.6153961	1.5601004	.8370792	49	42	.62402	1.599436	.8319541	18
12	.5485635	.6154375	1.5601226	.8368719	48	43	.62420	1.598490	.8317927	17
13	.5489070	.6154789	1.5601448	.8366605	47	44	.62438	1.597544	.8316312	16
14	.5492506	.6155203	1.5601670	.8364456	46	45	.62456	1.596598	.8314696	15
15	.5495941	.6155617	1.5601892	.8362262	45	46	.62474	1.595652	.8313080	14
16	.5499377	.6156031	1.5602114	.8360030	44	47	.62492	1.594706	.8311463	13
17	.5502812	.6156445	1.5602336	.8357757	43	48	.62510	1.593760	.8309846	12
18	.5506248	.6156859	1.5602558	.8355484	42	49	.62528	1.592814	.8308226	11
19	.5509683	.6157273	1.5602780	.8353160	41	50	.62546	1.591868	.8306607	10
20	.5513119	.6157687	1.5603002	.8350787	40	51	.62564	1.590922	.8304987	9
21	.5516554	.6158101	1.5603224	.8348364	39	52	.62582	1.590000	.8303366	8
22	.5519989	.6158515	1.5603446	.8345891	38	53	.62600	1.589052	.8301745	7
23	.5523425	.6158929	1.5603668	.8343368	37	54	.62618	1.588106	.8300123	6
24	.5526860	.6159343	1.5603890	.8340795	36	55	.62636	1.587159	.8298500	5
25	.5530295	.6159757	1.5604112	.8338172	35	56	.62654	1.586213	.8296877	4
26	.5533730	.6160171	1.5604334	.8335500	34	57	.62672	1.585267	.8295252	3
27	.5537165	.6160585	1.5604556	.8332777	33	58	.62690	1.584321	.8293628	2
28	.5540600	.6160999	1.5604778	.8330000	32	59	.62708	1.583375	.8292002	1
29	.5544035	.6161413	1.5605000	.8327177	31	60	.62726	1.582429	.8290376	0
30	.5547470	.6161827	1.5605222	.8324300	30					

Deg. 56.

Deg. 56.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

34 Deg.

34 Deg.

/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/
0	.5591929	.6745081	1.482261	.8290376	60	.31	.6060459	.687709	1.454102	28
1	.5594340	.674931	1.481631	.8288749	59	32	.6068586	.688137	1.453197	29
2	.5596751	.675355	1.481002	.8287121	58	33	.6076712	.688566	1.452292	27
3	.5599162	.675779	1.479773	.8285493	57	34	.6084838	.688995	1.451388	26
4	.5601572	.676202	1.478546	.8283864	56	35	.6092964	.689424	1.450485	25
5	.5603981	.676626	1.477319	.8282234	55	36	.6101090	.689853	1.449582	24
6	.5606390	.677050	1.476093	.8280603	54	37	.6109216	.690283	1.448680	23
7	.5608798	.677475	1.474868	.8278972	53	38	.6117342	.690712	1.447779	22
8	.5611206	.677899	1.473644	.8277340	52	39	.6125468	.691142	1.446879	21
9	.5613614	.678324	1.472421	.8275708	51	40	.6133594	.691572	1.445980	20
10	.5616021	.678749	1.471198	.8274074	50	41	.6141720	.692002	1.445081	19
11	.5618428	.679174	1.472576	.8272440	49	42	.6149846	.692432	1.444183	18
12	.5620834	.679599	1.471455	.8270806	48	43	.6157972	.692863	1.443286	17
13	.5623239	.680024	1.470333	.8269171	47	44	.6166098	.693293	1.442389	16
14	.5625645	.680450	1.469212	.8267534	46	45	.6174224	.693724	1.441494	15
15	.5628049	.680875	1.468090	.8265897	45	46	.6182350	.694155	1.440599	14
16	.5630453	.681301	1.466968	.8264260	44	47	.6190476	.694586	1.439704	13
17	.5632857	.681727	1.465845	.8262622	43	48	.6198602	.695018	1.438811	12
18	.5635260	.682153	1.464723	.8260983	42	49	.6206728	.695449	1.437918	11
19	.5637663	.682580	1.463600	.8259343	41	50	.6214854	.695881	1.437025	10
20	.5640066	.683006	1.462478	.8257703	40	51	.6222980	.696313	1.436135	9
21	.5642467	.683433	1.461354	.8256062	39	52	.6231106	.696745	1.435245	8
22	.5644869	.683860	1.460232	.8254420	38	53	.6239232	.697177	1.434355	7
23	.5647270	.684287	1.459107	.8252778	37	54	.6247358	.697609	1.433466	6
24	.5649670	.684714	1.457982	.8251135	36	55	.6255484	.698042	1.432578	5
25	.5652070	.685141	1.456857	.8249491	35	56	.6263610	.698474	1.431690	4
26	.5654469	.685568	1.455732	.8247847	34	57	.6271736	.698907	1.430803	3
27	.5656868	.685996	1.454607	.8246202	33	58	.6279862	.699340	1.429915	2
28	.5659267	.686424	1.453482	.8244556	32	59	.6287988	.699774	1.429027	1
29	.5661665	.686852	1.452357	.8242910	31	60	.6296114	.700207	1.428138	0
30	.5664062	.687281	1.451232	.8241262	30					

DEG. 56.

DEG. 55

NATURAL SINES AND TANGENTS TO A RADIUS 1.

85 Deg.

35 Deg.

/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/
0	5735764	700207	1.428148	8191520	31	5800397	713732	1.401086	8130466	29
1	5738147	700641	1.427284	8189852	32	5811765	714171	1.400224	8127775	28
2	5740529	701078	1.426381	8188182	33	5811765	714610	1.399363	8125084	27
3	5742911	701518	1.425498	8186512	34	5818864	715050	1.398503	8122393	26
4	5745292	701943	1.424617	8184841	35	5818864	715489	1.397644	8119701	25
5	5747672	702377	1.423736	8183169	36	5822530	715929	1.396785	8117008	24
6	5750053	702811	1.422856	8181497	37	5822530	716369	1.395927	8114314	23
7	5752432	703246	1.421976	8179824	38	5825959	716810	1.395069	8111621	22
8	5754811	703681	1.421097	8178151	39	5825959	717250	1.394213	8108928	21
9	5757190	704116	1.420220	8176476	40	5830687	717691	1.393357	8106235	20
10	5759568	704551	1.419342	8174801	41	5830687	718131	1.392501	8103542	19
11	5761946	704986	1.418466	8173125	42	5835412	718572	1.391647	8100849	18
12	5764323	705422	1.417590	8171449	43	5835412	719014	1.390793	8098156	17
13	5766700	705858	1.416715	8169772	44	5840135	719455	1.389940	8095463	16
14	5769076	706294	1.415840	8168094	45	5842497	719897	1.389087	8092770	15
15	5771452	706730	1.414967	8166416	46	5842497	720338	1.388235	8090077	14
16	5773827	707166	1.414094	8164736	47	5847217	720780	1.387384	8087384	13
17	5776202	707602	1.413222	8163056	48	5847217	721222	1.386534	8084691	12
18	5778576	708039	1.412350	8161376	49	5851935	721665	1.385684	8082000	11
19	5780950	708476	1.411479	8159695	50	5851935	722107	1.384835	8079308	10
20	5783323	708913	1.410609	8158013	51	5856652	722550	1.383986	8076616	9
21	5785696	709350	1.409740	8156330	52	5856652	722993	1.383139	8073924	8
22	5788069	709787	1.408871	8154647	53	5861367	723436	1.382292	8071232	7
23	5790440	710225	1.408003	8152963	54	5861367	723879	1.381445	8068540	6
24	5792812	710663	1.407136	8151278	55	5866080	724322	1.380600	8065848	5
25	5795183	711100	1.406270	8149593	56	5866080	724766	1.379755	8063156	4
26	5797553	711539	1.405404	8147906	57	5868435	725210	1.378910	8060464	3
27	5799923	711977	1.404539	8146220	58	5871070	725654	1.378067	8057772	2
28	5802292	712415	1.403674	8144532	59	5871070	726098	1.377224	8055080	1
29	5804661	712854	1.402811	8142844	60	5877853	726542	1.376381	8052388	0
30	5807030	713293	1.401948	8141155	30				8049696	

Deg. 54.

Deg. 54.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

36 Deg.

36 Deg.

/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/
0	.5877853	.726542	1.376381	.8090170	60	.31	.740411	1.330600	.8036838	29
1	.5880206	.726587	1.376540	.8088460	59	32	.740891	1.330779	.8035107	28
2	.5882558	.727431	1.377469	.8086749	58	33	.741312	1.330958	.8033375	27
3	.5884910	.727876	1.378389	.8085037	57	34	.741763	1.331139	.8031642	26
4	.5887262	.728321	1.379319	.8083325	56	35	.742214	1.331319	.8029909	25
5	.5889613	.728767	1.372180	.8081612	55	36	.742665	1.331501	.8028175	24
6	.5891964	.729212	1.371342	.8079899	54	37	.743117	1.331683	.8026440	23
7	.5894314	.729658	1.370504	.8078185	53	38	.743568	1.331865	.8024705	22
8	.5896663	.730104	1.369667	.8076470	52	39	.744020	1.332049	.8022969	21
9	.5899012	.730551	1.368831	.8074754	51	40	.744472	1.332233	.8021232	20
10	.5901361	.731006	1.367995	.8073038	50	41	.744924	1.332417	.8019495	19
11	.5903709	.731461	1.367161	.8071321	49	42	.745377	1.332602	.8017756	18
12	.5906057	.731919	1.366326	.8069603	48	43	.745829	1.332788	.8016018	17
13	.5908404	.732386	1.365493	.8067885	47	44	.746282	1.332975	.8014278	16
14	.5910750	.732853	1.364660	.8066166	46	45	.746735	1.333162	.8012538	15
15	.5913096	.733320	1.363827	.8064446	45	46	.747188	1.333350	.8010797	14
16	.5915442	.733787	1.362996	.8062726	44	47	.747642	1.333538	.8009056	13
17	.5917787	.734255	1.362165	.8061005	43	48	.748095	1.333727	.8007314	12
18	.5920132	.734725	1.361335	.8059283	42	49	.748549	1.333917	.8005571	11
19	.5922476	.735192	1.360505	.8057560	41	50	.749003	1.334107	.8003827	10
20	.5924819	.735661	1.359676	.8055837	40	51	.749457	1.334298	.8002083	9
21	.5927163	.736130	1.358848	.8054113	39	52	.749911	1.334490	.8000338	8
22	.5929505	.736596	1.358020	.8052389	38	53	.750366	1.334682	.7998593	7
23	.5931847	.737064	1.357193	.8050664	37	54	.750821	1.334875	.7996847	6
24	.5934189	.737533	1.356367	.8048938	36	55	.751276	1.335068	.7995100	5
25	.5936530	.737999	1.355541	.8047211	35	56	.751731	1.335262	.7993352	4
26	.5938871	.738468	1.354716	.8045484	34	57	.752186	1.335457	.7991604	3
27	.5941211	.738931	1.353891	.8043756	33	58	.752642	1.335653	.7989855	2
28	.5943550	.739396	1.353068	.8042028	32	59	.753098	1.335850	.7988105	1
29	.5945889	.739861	1.352244	.8040299	31	60	.753554	1.336048	.7986355	0
30	.5948228	.739961	1.351422	.8038569	30					

Dga. 53.

Dga. 53.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

37 DEG.

37 DEG.

/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/
0	.6018150	.753554	1.327044	.7985355	60	.31	.6080922	.767789	.7931762	29
1	.6020473	.754010	1.326242	.7984604	59	32	.6092220	.768251	.7929900	28
2	.6022795	.754466	1.325439	.7983853	58	33	.6094535	.768714	.7928218	27
3	.6025117	.754923	1.324638	.7983100	57	34	.6096841	.769177	.7926545	26
4	.6027439	.755379	1.323837	.7979347	56	35	.6099147	.769640	.7924871	25
5	.6029760	.755836	1.323036	.7977594	55	36	.6101452	.770103	.7923206	24
6	.6032080	.756294	1.322237	.7975839	54	37	.6103756	.770567	.7921541	23
7	.6034400	.756751	1.321437	.7974084	53	38	.6106060	.771030	.7919876	22
8	.6036719	.757209	1.320639	.7972329	52	39	.6108363	.771494	.7918211	21
9	.6039038	.757666	1.319841	.7970572	51	40	.6110666	.771958	.7916546	20
10	.6041356	.758124	1.319044	.7968815	50	41	.6112969	.772423	.7914881	19
11	.6043674	.758582	1.318247	.7967058	49	42	.6115270	.772887	.7913216	18
12	.6045991	.759041	1.317451	.7965299	48	43	.6117572	.773352	.7911551	17
13	.6048308	.759499	1.316655	.7963540	47	44	.6119873	.773817	.7909886	16
14	.6050624	.759958	1.315861	.7961780	46	45	.6122173	.774282	.7908221	15
15	.6052940	.760417	1.315066	.7960020	45	46	.6124473	.774748	.7906556	14
16	.6055255	.760876	1.314273	.7958259	44	47	.6126772	.775213	.7904891	13
17	.6057570	.761336	1.313480	.7956497	43	48	.6129071	.775679	.7903226	12
18	.6059884	.761795	1.312687	.7954735	42	49	.6131369	.776145	.7901561	11
19	.6062198	.762253	1.311895	.7952972	41	50	.6133666	.776611	.7899896	10
20	.6064511	.762715	1.311104	.7951208	40	51	.6135964	.777078	.7898231	9
21	.6066824	.763175	1.310314	.7949444	39	52	.6138260	.777544	.7896566	8
22	.6069136	.763635	1.309523	.7947678	38	53	.6140556	.778011	.7894901	7
23	.6071447	.764097	1.308734	.7945913	37	54	.6142852	.778478	.7893236	6
24	.6073758	.764557	1.307945	.7944146	36	55	.6145147	.778946	.7891571	5
25	.6076069	.765018	1.307157	.7942379	35	56	.6147442	.779413	.7889906	4
26	.6078379	.765480	1.306369	.7940611	34	57	.6149736	.779881	.7888241	3
27	.6080689	.765941	1.305582	.7938843	33	58	.6152029	.780349	.7886576	2
28	.6082998	.766403	1.304796	.7937074	32	59	.6154322	.780817	.7884911	1
29	.6085306	.766864	1.304010	.7935304	31	60	.6156615	.781285	.7883246	0
30	.6087614	.767327	1.303225	.7933533	30					

Deg. 52.

Deg. 52.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

38 Deg.

38 Deg.

/	SINE.	TANG.	COTANG.	COSINE.	/	SINE.	TANG.	COTANG.	COSINE.	/
0	.6156615	.781295	1.279941	.780108	60	.31	.6227423	7.95911	1.256421	782.970
1	.6158007	.781754	1.279174	.7878316	59	32	.6230938	7.96386	1.255672	782.249
2	.6161108	.782222	1.278407	.7876524	58	33	.6234474	7.96861	1.254922	781.528
3	.6164349	.782691	1.277641	.7874732	57	34	.6238029	7.97337	1.254174	780.803
4	.6167680	.783161	1.276876	.7872939	56	35	.6241592	7.97813	1.253426	780.079
5	.6168869	.783630	1.276111	.7871145	55	36	.6245166	7.98289	1.252678	781.520
6	.6170369	.784100	1.275347	.7869350	54	37	.6248740	7.98765	1.251931	781.330
7	.6172043	.784570	1.274583	.7867555	53	38	.6252314	7.99242	1.251184	781.157
8	.6174936	.785040	1.273820	.7865759	52	39	.6255888	7.99719	1.250438	780.975
9	.6177924	.785510	1.273057	.7863963	51	40	.6259462	8.00196	1.249693	780.794
10	.6179511	.785981	1.272295	.7862165	50	41	.6263036	8.00673	1.248948	780.613
11	.6181798	.786451	1.271534	.7860367	49	42	.6266610	8.01151	1.248204	780.430
12	.6184084	.786922	1.270773	.7858569	48	43	.6270184	8.01628	1.247460	780.248
13	.6186370	.787393	1.270013	.7856770	47	44	.6273758	8.02106	1.246716	780.065
14	.6188655	.787864	1.269253	.7854970	46	45	.6277332	8.02584	1.245974	779.884
15	.6190939	.788336	1.268494	.7853169	45	46	.6280906	8.03063	1.245232	779.702
16	.6193224	.788808	1.267735	.7851368	44	47	.6284479	8.03541	1.244490	779.520
17	.6195507	.789280	1.266977	.7849566	43	48	.6288053	8.04020	1.243749	779.338
18	.6197790	.789752	1.266219	.7847764	42	49	.6291627	8.04499	1.243008	779.157
19	.6200073	.790224	1.265462	.7845961	41	50	.6295201	8.04979	1.242268	778.975
20	.6202355	.790697	1.264706	.7844157	40	51	.6298775	8.05458	1.241529	778.793
21	.6204636	.791170	1.263950	.7842352	39	52	.6302349	8.05938	1.240790	778.611
22	.6206917	.791643	1.263195	.7840547	38	53	.6305923	8.06418	1.240051	778.429
23	.6209198	.792116	1.262440	.7838741	37	54	.6309497	8.06898	1.239313	778.243
24	.6211478	.792590	1.261686	.7836935	36	55	.6313071	8.07378	1.238576	778.060
25	.6213757	.793064	1.260932	.7835127	35	56	.6316645	8.07859	1.237839	777.877
26	.6216036	.793537	1.260179	.7833320	34	57	.6320219	8.08340	1.237103	777.694
27	.6218314	.794012	1.259426	.7831511	33	58	.6323793	8.08821	1.236367	777.512
28	.6220592	.794486	1.258674	.7829702	32	59	.6327367	8.09302	1.235631	777.329
29	.6222870	.794961	1.257923	.7827892	31	60	.6330941	8.09784	1.234897	777.146
30	.6225145	.795435	1.257172	.7826082	30					

Deg. 51.

Deg. 51.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

39 Deg.

39 Deg.

/	SINE.	TANG.	COTANG.	COSINE.	/	/	SINE.	TANG.	COTANG.	COSINE.	/
0	.0000000	.0000000		.7771440	60	31	.6330266	.824825		.7714395	29
1	.0086959	.0154005	1.234162	.7769629	59	32	.6325270	.8253114	1.212378	.7712544	28
2	.0173612	.0307724	1.233429	.7767797	58	33	.6320276	.8258003	1.211660	.7710692	27
3	.0260165	.0461430	1.232696	.7765965	57	34	.6315282	.8262922	1.210942	.7708840	26
4	.0346718	.0615138	1.231963	.7764132	56	35	.6310288	.8267822	1.210225	.7706986	25
5	.0433271	.0768846	1.231231	.7762298	55	36	.6305294	.8272721	1.209508	.7705132	24
6	.0519824	.0922554	1.230499	.7760464	54	37	.6300300	.8277622	1.208792	.7703278	23
7	.0606377	.1076262	1.229768	.7758629	53	38	.6295306	.8282522	1.208076	.7701423	22
8	.0692930	.1229970	1.229038	.7756794	52	39	.6290312	.8287422	1.207361	.7699567	21
9	.0779483	.1383678	1.228308	.7754957	51	40	.6285318	.8292322	1.206646	.7697710	20
10	.0866036	.1537386	1.227578	.7753121	50	41	.6280324	.8297222	1.205932	.7695853	19
11	.0952589	.1691094	1.226849	.7751283	49	42	.6275330	.8302122	1.205219	.7693996	18
12	.1039142	.1844802	1.226121	.7749445	48	43	.6270336	.8307022	1.204505	.7692137	17
13	.1125695	.2000000	1.225393	.7747606	47	44	.6265342	.8311922	1.203793	.7690278	16
14	.1212248	.2155196	1.224665	.7745767	46	45	.6260348	.8316822	1.203081	.7688418	15
15	.1298801	.2310392	1.223938	.7743926	45	46	.6255354	.8321722	1.202369	.7686558	14
16	.1385354	.2465588	1.223212	.7742086	44	47	.6250360	.8326622	1.201657	.7684697	13
17	.1471907	.2620784	1.222486	.7740244	43	48	.6245366	.8331522	1.200945	.7682835	12
18	.1558460	.2775980	1.221761	.7738402	42	49	.6240372	.8336422	1.200233	.7680973	11
19	.1645013	.2931176	1.221036	.7736559	41	50	.6235378	.8341322	1.199521	.7679110	10
20	.1731566	.3086372	1.220312	.7734716	40	51	.6230384	.8346222	1.198818	.7677246	9
21	.1818119	.3241568	1.219588	.7732872	39	52	.6225390	.8351122	1.198109	.7675382	8
22	.1904672	.3396764	1.218865	.7731027	38	53	.6220396	.8356022	1.197401	.7673517	7
23	.1991225	.3551960	1.218141	.7729182	37	54	.6215402	.8360922	1.196693	.7671652	6
24	.2077778	.3707156	1.217419	.7727336	36	55	.6210408	.8365822	1.195986	.7669785	5
25	.2164331	.3862352	1.216698	.7725489	35	56	.6205414	.8370722	1.195279	.7667918	4
26	.2250884	.4017548	1.215976	.7723642	34	57	.6200420	.8375622	1.194573	.7666051	3
27	.2337437	.4172744	1.215255	.7721794	33	58	.6195426	.8380522	1.193867	.7664183	2
28	.2423990	.4327940	1.214533	.7719945	32	59	.6190432	.8385422	1.193162	.7662314	1
29	.2510543	.4483136	1.213816	.7718096	31	60	.6185438	.8390322	1.192457	.7660444	0
30	.2597096	.4638332	1.213097	.7716246	30				1.191753		

Deg. 50.

Deg. 50.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

40 Deg.

40 Deg.

/	SINE.	TANG.	COTANG.	COSINE.	/	/	SINE.	TANG.	COTANG.	COSINE.	/
0	.6427576	839099	1.191753	.7660444	60	31	.6466392	.854583	1.170160	.7602170	29
1	.6430104	839505	1.191049	.7658574	59	32	.6468903	.855087	1.169471	.7600280	28
2	.6432332	840091	1.190346	.7656704	58	33	.6501114	.855591	1.168782	.7598389	27
3	.6434559	840587	1.189643	.7654832	57	34	.6503523	.856095	1.168094	.7596498	26
4	.6436785	841084	1.188941	.7652960	56	35	.6505932	.856599	1.167407	.7594606	25
5	.6439011	841581	1.188239	.7651087	55	36	.6508341	.857103	1.166720	.7592713	24
6	.6441236	842078	1.187538	.7649214	54	37	.6510750	.857608	1.166033	.7590820	23
7	.6443461	842575	1.186837	.7647340	53	38	.6513158	.858113	1.165347	.7588926	22
8	.6445685	843073	1.186136	.7645465	52	39	.6515567	.858618	1.164661	.7587031	21
9	.6447909	843570	1.185437	.7643590	51	40	.6517975	.859124	1.163976	.7585136	20
10	.6450132	844068	1.184737	.7641714	50	41	.6520384	.859629	1.163291	.7583240	19
11	.6452355	844567	1.184038	.7639838	49	42	.6522793	.860135	1.162607	.7581343	18
12	.6454577	845065	1.183340	.7637960	48	43	.6525202	.860641	1.161923	.7579446	17
13	.6456798	845564	1.182642	.7636082	47	44	.6527611	.861148	1.161240	.7577548	16
14	.6459019	846063	1.181944	.7634204	46	45	.6530020	.861655	1.160557	.7575650	15
15	.6461240	846562	1.181247	.7632325	45	46	.6532429	.862162	1.159874	.7573751	14
16	.6463460	847061	1.180551	.7630445	44	47	.6534838	.862669	1.159192	.7571851	13
17	.6465679	847561	1.179855	.7628564	43	48	.6537247	.863176	1.158511	.7569951	12
18	.6467898	848061	1.179159	.7626683	42	49	.6539656	.863684	1.157830	.7568050	11
19	.6470116	848561	1.178464	.7624802	41	50	.6542065	.864192	1.157149	.7566148	10
20	.6472334	849062	1.177769	.7622921	40	51	.6544474	.864700	1.156469	.7564246	9
21	.6474551	849563	1.177075	.7621039	39	52	.6546883	.865209	1.155789	.7562343	8
22	.6476767	850064	1.176382	.7619157	38	53	.6549292	.865718	1.155110	.7560439	7
23	.6478984	850565	1.175688	.7617276	37	54	.6551701	.866227	1.154431	.7558535	6
24	.6481199	851066	1.174993	.7615395	36	55	.6554110	.866736	1.153753	.7556630	5
25	.6483414	851568	1.174303	.7613513	35	56	.6556519	.867246	1.153075	.7554724	4
26	.6485628	852070	1.173612	.7611631	34	57	.6558928	.867755	1.152397	.7552818	3
27	.6487842	852572	1.172921	.7609749	33	58	.6561337	.868265	1.151721	.7550911	2
28	.6490056	853075	1.172229	.7607867	32	59	.6563746	.868776	1.151044	.7549004	1
29	.6492268	853577	1.171539	.7605984	31	60	.6566155	.869286	1.150368	.7547096	0
30	.6494480	854080	1.170849	.7604100	30						

Deg. 49.

Deg. 49.

NATURAL SINES AND TANGENTS TO A RADIUS 1.

41 DEG.

41 DEG.

/	/	SINE.	TANG.	COTANG.	COSINE.	/	/	SINE.	TANG.	COTANG.	COSINE.	/	/
0	0	6560590	87286	1-150368	7547096	60	31	6623579	88524	1-129632	7487629	20	20
1	1	6562785	869797	1-149692	7545187	59	32	6630357	885763	1-128970	7485701	21	21
2	2	6564980	870308	1-149017	7543278	58	33	6637134	886282	1-128308	7483772	22	22
3	3	6567174	870820	1-148342	7541368	57	34	6643910	886801	1-127647	7481842	23	23
4	4	6569367	871331	1-147668	7539457	56	35	6650687	887321	1-126987	7479912	24	24
5	5	6571560	871843	1-146994	7537546	55	36	6657463	887841	1-126327	7477981	25	25
6	6	6573752	872355	1-146321	7535635	54	37	6664239	888361	1-125667	7476050	26	26
7	7	6575944	872868	1-145648	7533724	53	38	6671015	888882	1-125008	7474119	27	27
8	8	6578135	873380	1-144976	7531808	52	39	6677791	889403	1-124349	7472188	28	28
9	9	6580326	873893	1-144304	7529894	51	40	6684568	889924	1-123690	7470257	29	29
10	10	6582516	874406	1-143632	7527980	50	41	6691344	890445	1-123032	7468326	30	30
11	11	6584706	874920	1-142960	7526065	49	42	6698120	890967	1-122375	7466395	31	31
12	12	6586896	875433	1-142289	7524149	48	43	6704896	891489	1-121718	7464464	32	32
13	13	6589085	875947	1-141620	7522233	47	44	6711672	892011	1-121061	7462533	33	33
14	14	6591271	876462	1-140951	7520316	46	45	6718448	892534	1-120405	7460602	34	34
15	15	6593458	876976	1-140281	7518398	45	46	6725224	893056	1-119749	7458671	35	35
16	16	6595645	877491	1-139612	7516480	44	47	6732000	893579	1-119094	7456740	36	36
17	17	6597831	878006	1-138944	7514561	43	48	6738776	894103	1-118439	7454809	37	37
18	18	6600017	878521	1-138276	7512641	42	49	6745552	894626	1-117784	7452878	38	38
19	19	6602202	879037	1-137608	7510721	41	50	6752328	895150	1-117130	7450947	39	39
20	20	6604386	879552	1-136941	7508800	40	51	6759104	895674	1-116476	7449016	40	40
21	21	6606570	880068	1-136274	7506879	39	52	6765880	896199	1-115823	7447085	41	41
22	22	6608754	880585	1-135608	7504957	38	53	6772656	896723	1-115170	7445154	42	42
23	23	6610936	881101	1-134942	7503034	37	54	6779432	897248	1-114518	7443223	43	43
24	24	6613119	881618	1-134277	7501111	36	55	6786208	897773	1-113866	7441292	44	44
25	25	6615300	882135	1-133612	7499187	35	56	6792984	898299	1-113214	7439361	45	45
26	26	6617482	882653	1-132947	7497262	34	57	6799760	898825	1-112563	7437430	46	46
27	27	6619662	883170	1-132283	7495337	33	58	6806536	899351	1-111912	7435500	47	47
28	28	6621842	883688	1-131620	7493411	32	59	6813312	899877	1-111262	7433570	48	48
29	29	6624022	884206	1-130957	7491484	31	60	6820088	900404	1-110612	7431640	49	49
30	30	6626200	884725	1-130294	7489557	30						50	50

Deg. 48.

Deg. 48.

